

# InterOPERA 2<sup>nd</sup> dissemination event

“Towards the interoperability of multi-vendor HVDC grids”

# AGENDA

15.00 – 15.05	<b>Welcome</b> <ul style="list-style-type: none"><li>Sébastien Silvant, Supergrid Institute</li></ul>
15.05 – 15.15	<b>Keynote speech</b> <ul style="list-style-type: none"><li>Eric Lecomte, DG Energy, European Commission</li></ul>
15.15 – 15.35	<b>InterOPERA Phase I – What we've achieved so far</b> <ul style="list-style-type: none"><li>Patrick Düllmann, Siemens Energy</li><li>Carmen Cardozo, RTE</li></ul>
15.35 – 15.55	<b>InterOPERA Phase II – What's coming next</b> <ul style="list-style-type: none"><li>Oliver Pohl, Amprion</li><li>René Lindeboom, Ørsted</li></ul>
15.55 – 16.00	<b>Closing remarks</b> <ul style="list-style-type: none"><li>Riccardo Longo, WindEurope</li></ul>

Questions?

Contact us at  
[info@interopera.eu](mailto:info@interopera.eu)

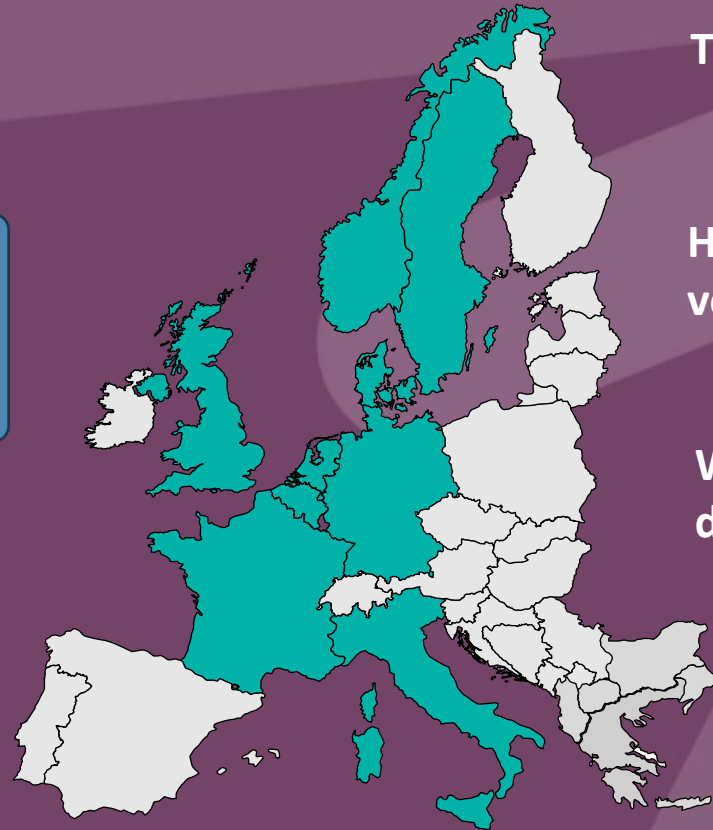
Start date  
1 January 2023

End date  
30 April 2027

Main target:  
To enable multi-vendor HVDC grids in Europe

70 M€ budget

EU contribution  
~ 50 M€



TSOs



HVDC vendors



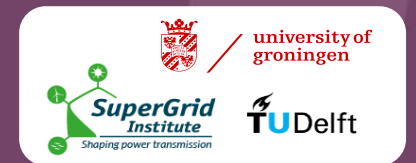
Wind developers



WTG vendors



Research & innovation



Technical frameworks (*functional specs, grid design, Demonstrator*)  
+ Non-technical frameworks (*procurement, cooperation, regulation*)  
= Real-world deployment of multi-vendor HVDC grids in Europe.

Coordinated by  
SuperGrid Institute (France)  
Grant Agreement 101095874

PUBLIC

# InterOPERA Phase I

## What we've achieved so far

**WP3 – Multi-Terminal Multi-Vendor Demonstrator project**

**Task 3.3 – Demonstrator detailed functional specifications**

**Task 3.6 – Demonstrator HVDC grid design studies**

# 1

## Demonstrator detailed functional specifications

*Applying the InterOPERA functional framework to the demonstrator*

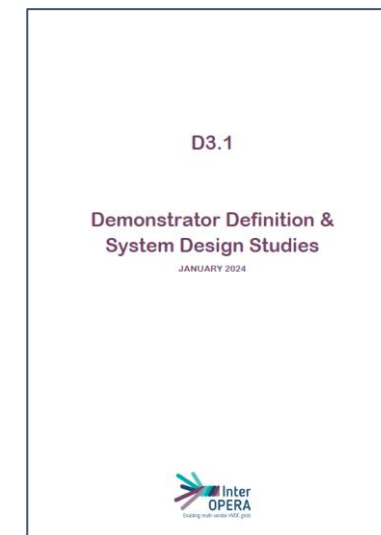
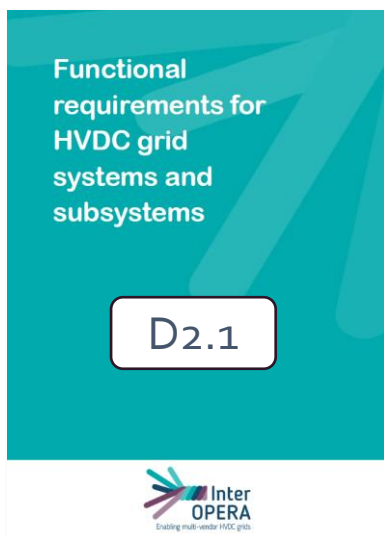
# From a functional framework → detailed specifications

Functional framework  
Basic subsystems requirements

Demonstrator definition & system  
objectives

Assign functions & capabilities to subsystems

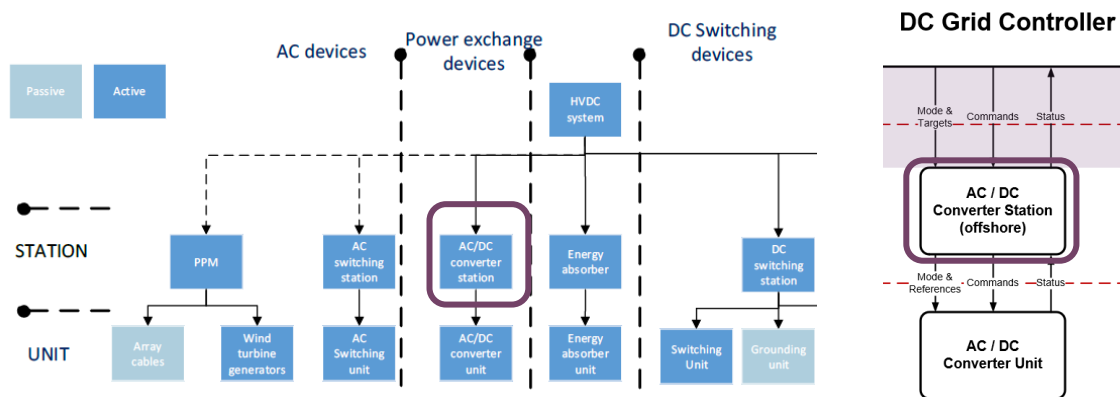
Detailed subsystems specifications  
at DC-POC (high voltage interfaces), incl. DC grid equivalents  
at communication interface (signal list)



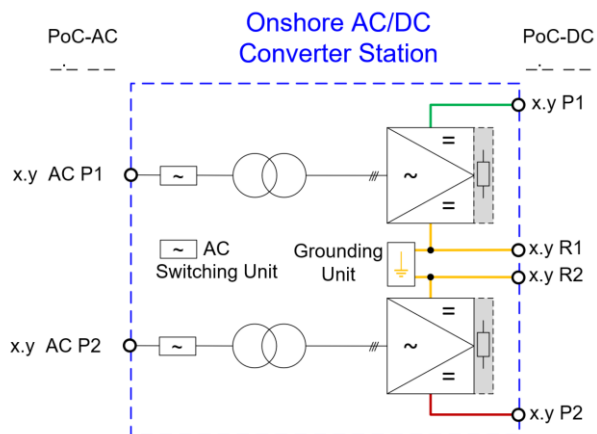
[interopera.eu/publications](https://interopera.eu/publications)

# Subsystem definition & InterOPERA Demonstrator (3T)

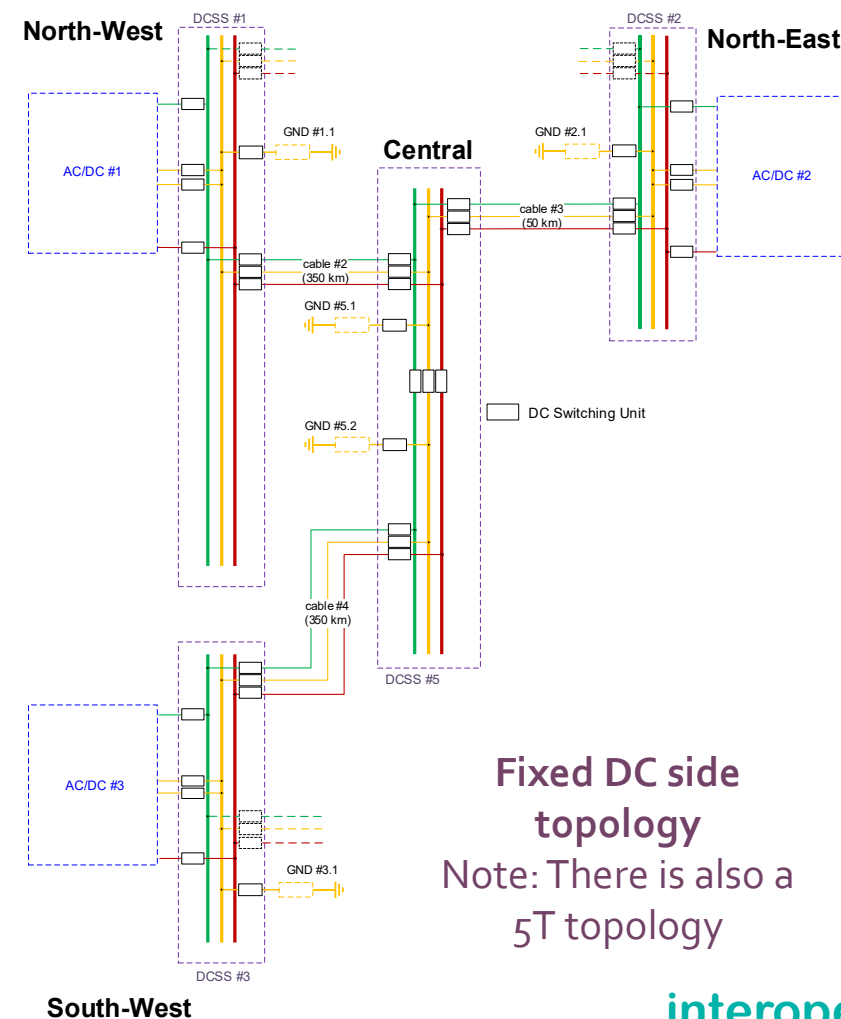
## Functional framework / architecture



Example:



## Demonstrator definition



**Fixed DC side topology**  
Note: There is also a 5T topology

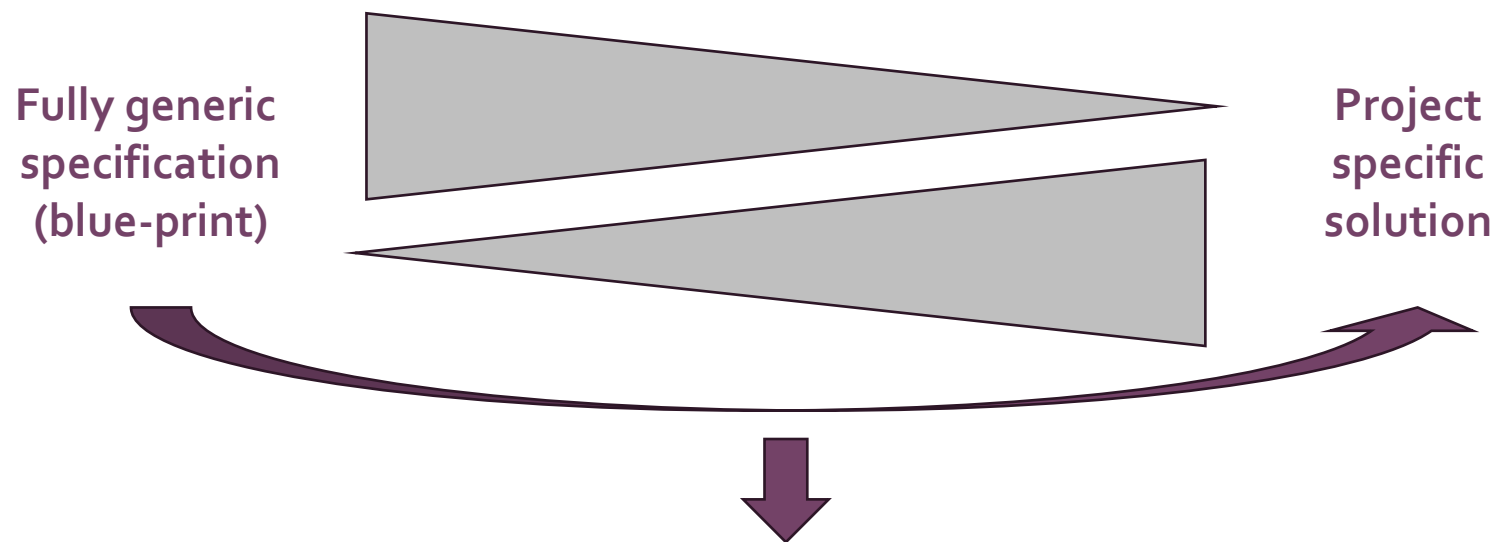
# From a functional framework → detailed specifications

## Needed: Detailed subsystem specification

- ❖ Includes specification of behaviour at the interfaces

## Challenges to be addressed:

- ❖ New and exploratory functionalities
- ❖ Realisation / development of technical solutions in a given time frame

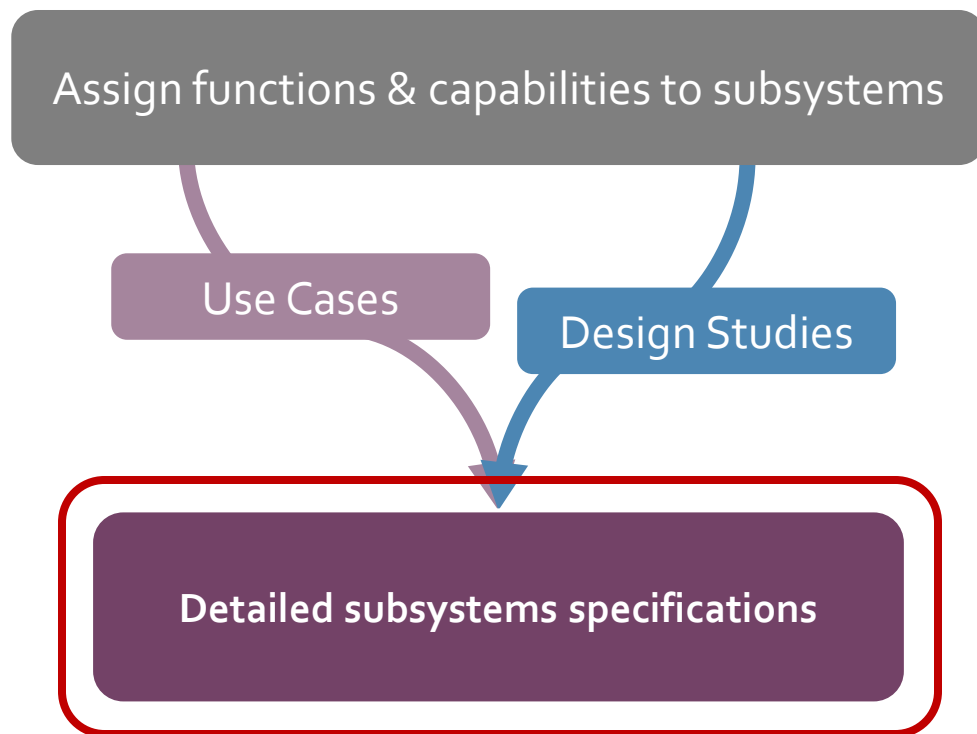


## Approach followed in InterOPERA : Close the gap

- Trade-off: As generic as possible, as specific to demo as needed
- Derive & Describe methodologies to create „system-specific“ specifications in line with the generic functional framework
- Allow updates to specifications after demonstrator studies



# Refine use cases & design parameters to close the gap!

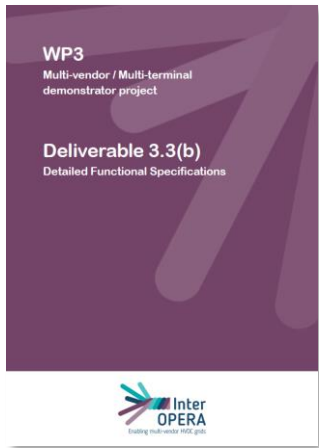


- We defined **use cases** to break down the InterOPERA project objectives into a functional framework
- We carried out **System-Level Design Studies** to specify the necessary design parameters e.g. voltage & current bands, operational limits, network control parameters & grid protection settings



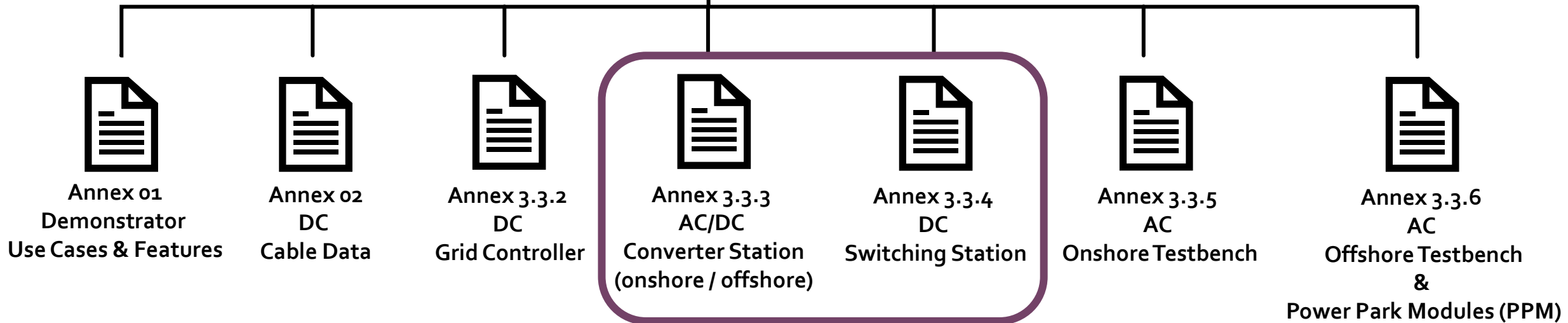
Second part of this presentation ☺

# Detailed Functional Specifications: Overview



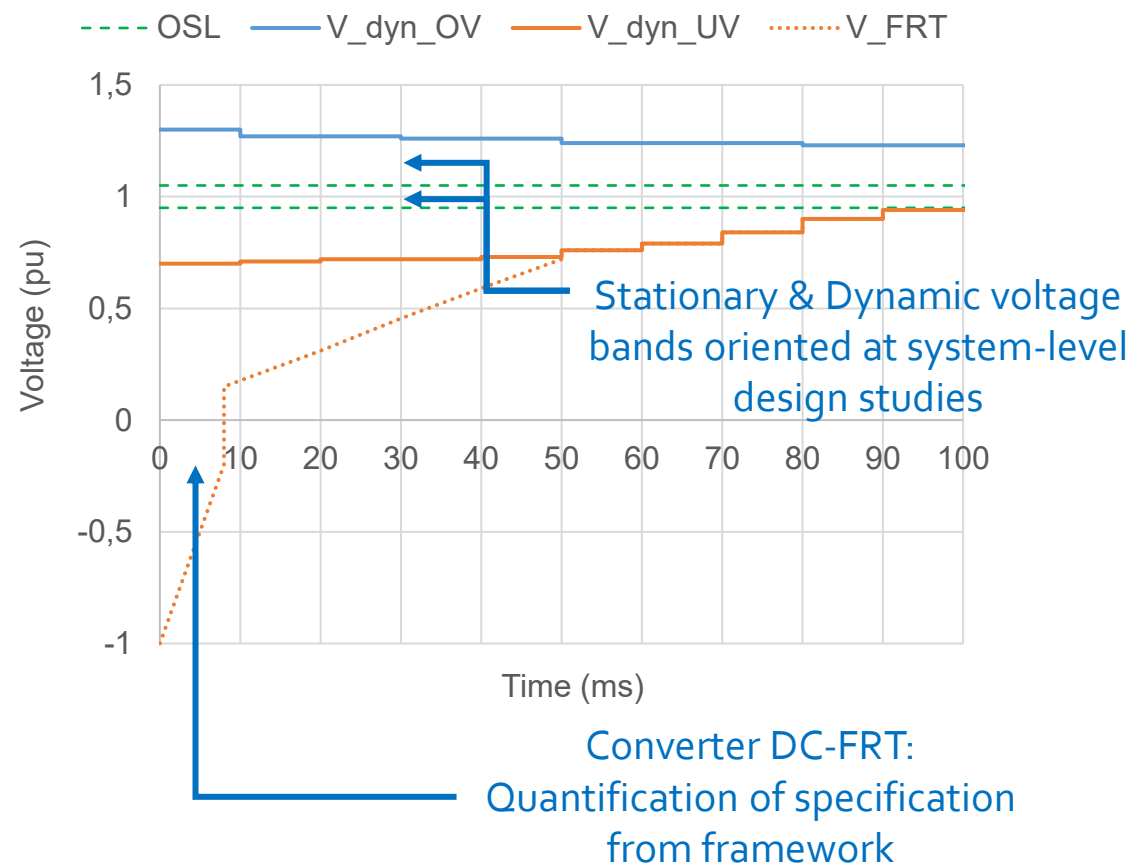
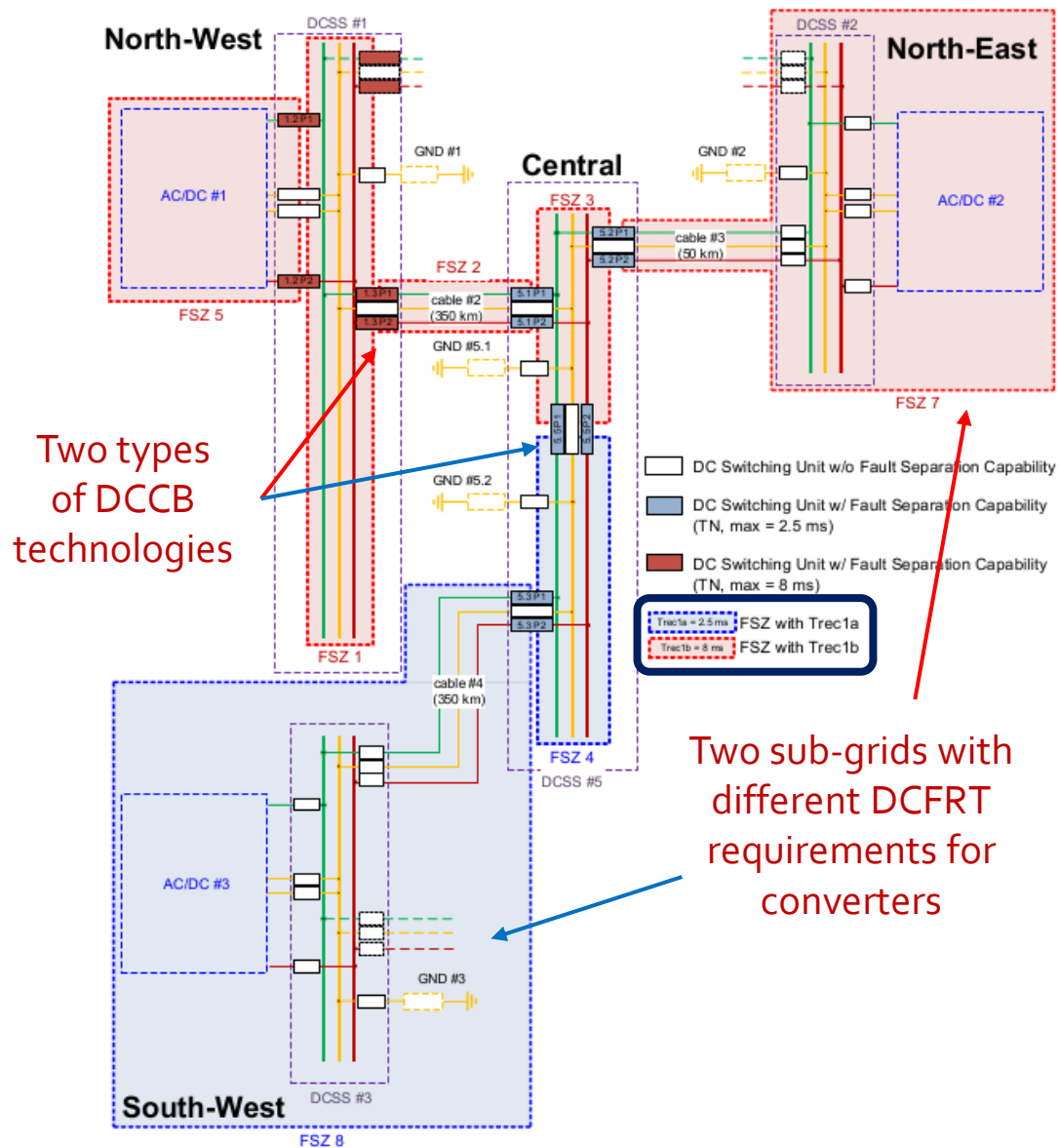
## Overall Demonstrator Definition

- Topology
- Grid Characteristics
- Control Philosophy
- Protection Philosophy



Example in the following

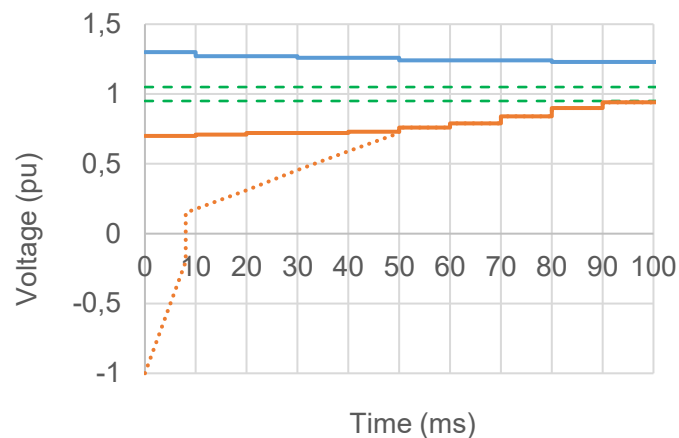
# Example: Specification of DC fault reactions



# Functionally split specifications for subsystems

## AC/DC converter station

Detailed specifications

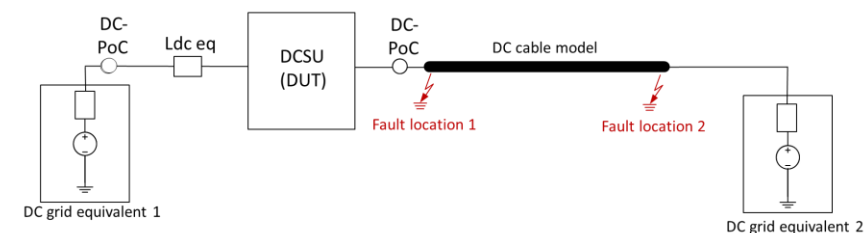
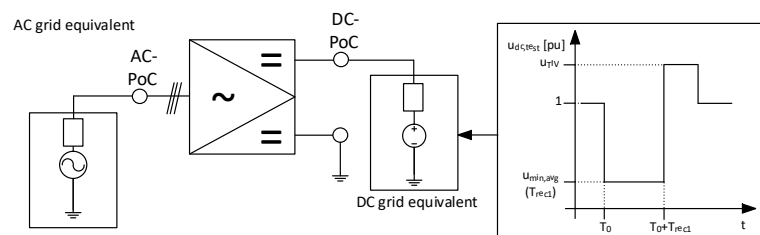


## DC switching station

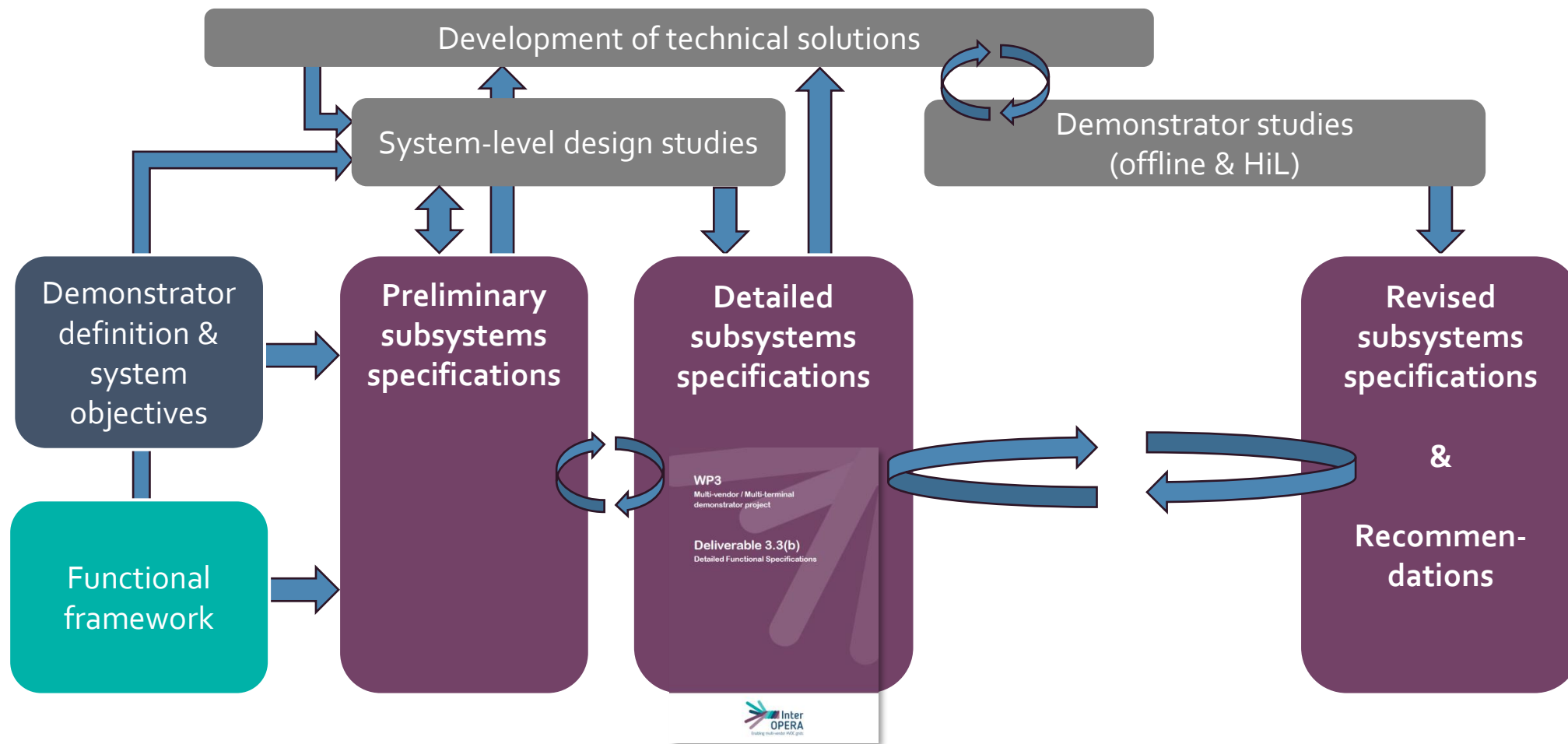
Table 4-3: DC switching unit functions (preliminary specifications)

Item #	Function	High voltage DC system ( $P_n$ )	Neutral DC system ( $R_n$ )
1	Maintenance earthing*	X	X
2	Transmission unit earthed**	X	X
3	Voltage isolation	X	X
4	Current making	X	X
5	Peak current suppression	X	
6	Residual current breaking	X	X
7	Fault separation	X	
8	On-load switching	X	
9	DC voltage measurement	X	X
10	DC current measurement	X	X
11	Fault zone identification	X	

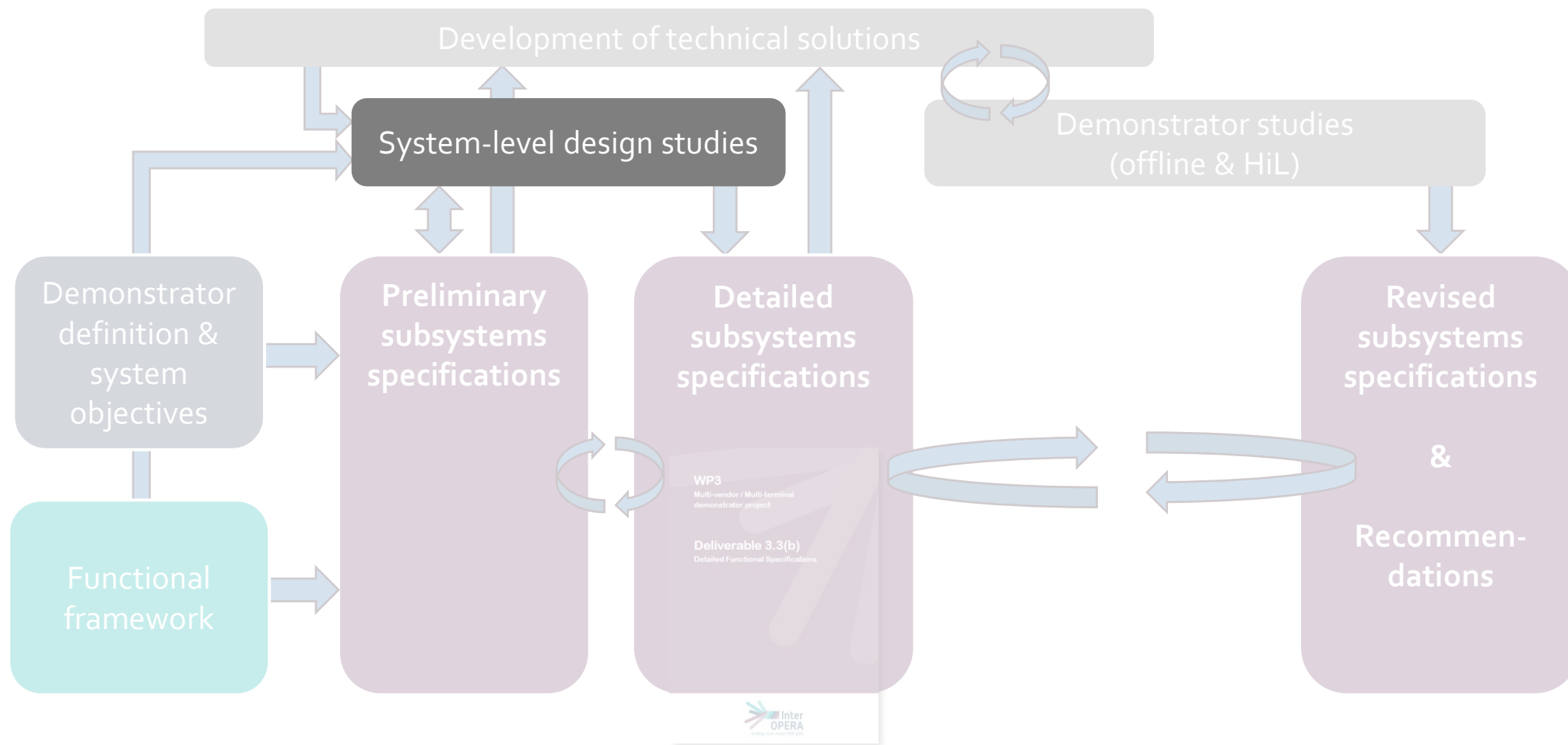
Standalone conformity tests



# Functional specification is an ongoing process



# Functional specification is an ongoing process



# 2

## Demonstrator HVDC grid design studies

*Quantifying electrical stress during contingencies to ensure demo reliable operation*

# What are HVDC grid design studies about?

**Early-stage**, system-level studies, based on **generic models** aimed to support detailed subsystem specifications, focusing on informing primary design decisions.

## Why do we need them?

New design constraints as we move from point-to-point links to multi-terminal grids

- P2P HVDC links have two states: operational (e.g., AC-FRT) & blackout (e.g., DC fault)
- MT HVDC systems, parts of the grid must survive terminal outages & DC disturbances

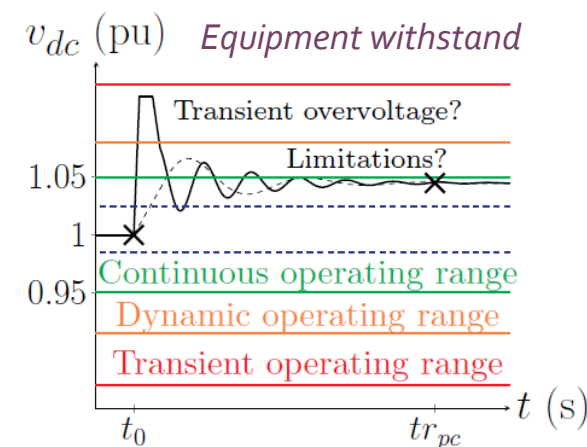
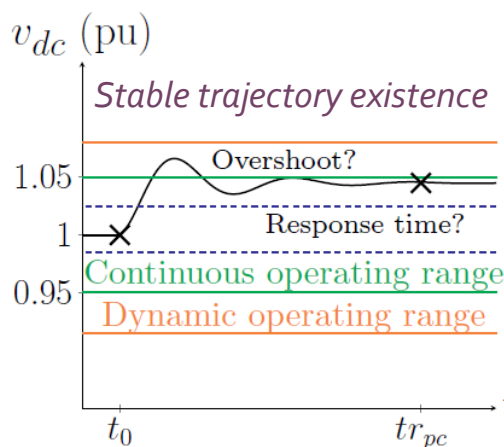
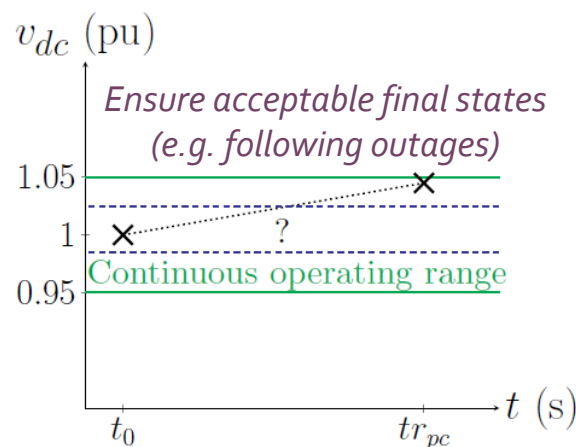
**The system must be *designed* for it!**



# How?

## A three-level study package

1. DC Load flow study & contingency analysis
2. Dynamic Study
3. Transient Study



**Challenge:** outcomes strongly depend on **key assumptions**, which must be technology-inclusive, conservative, yet reasonable.

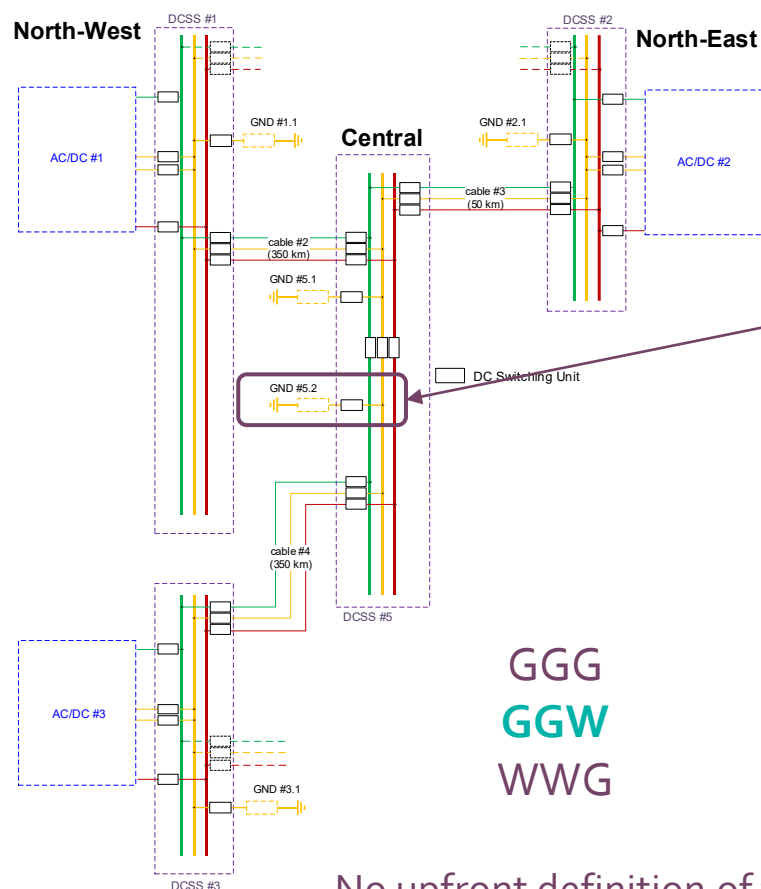
*Insufficient design space: incompatibilities*

*Risk of overdesign & technology exclusion*

Conservatism Level

# → We started with an assumption alignment phase

E.g. Continuous operating range [475 525] kV ([0.95 1.05] pu)

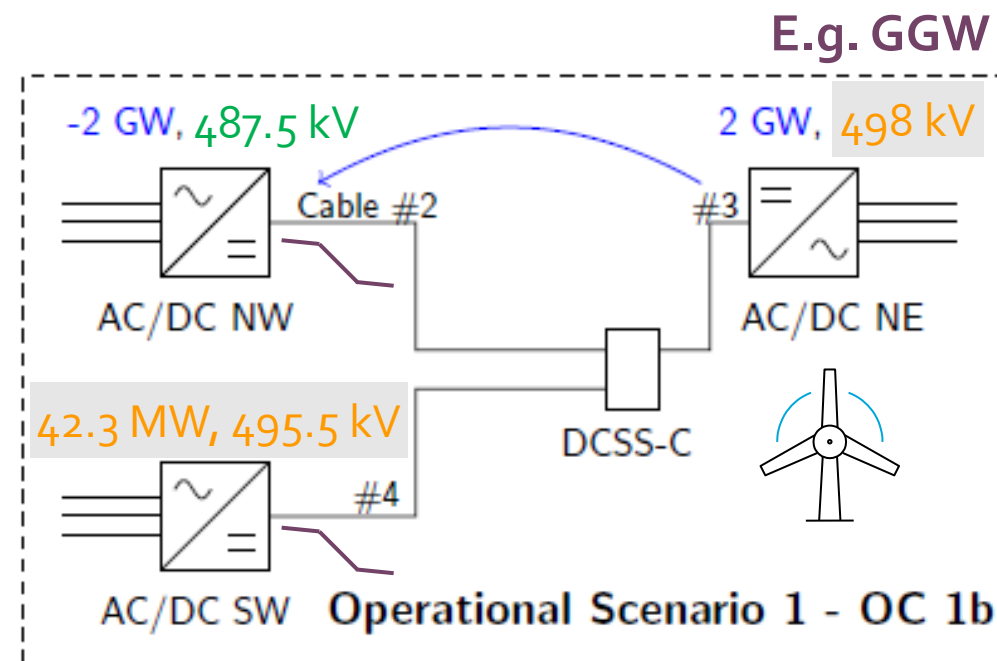


No upfront definition of the station type allowing for various configurations onshore / offshore

1. Agreement on system-level parameters and DC cable data<sup>1</sup>
2. Neutral system grounding at DCSS #5
3. AC grid connection assumptions
4. AC/DC converter capabilities (e.g. control)
5. DCCB capabilities (fault neutralisation time)
6. Fault separation zones & subgrid definition
7. Consideration of DC-FRT requirements

# 1 – DC Load Flow-based design study process

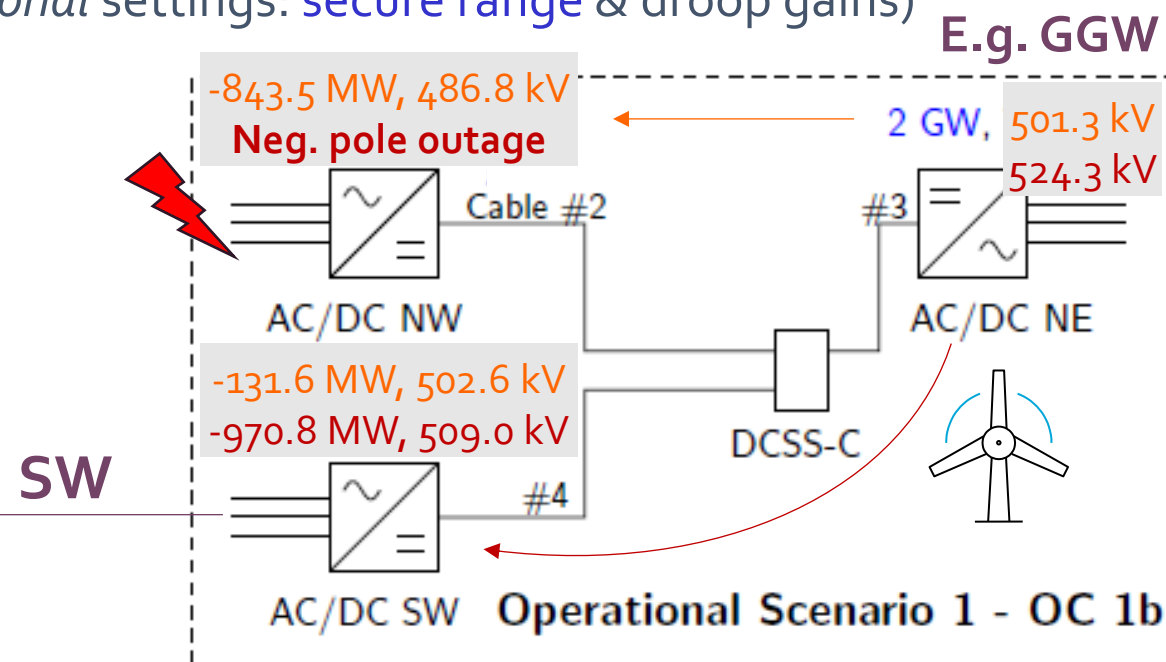
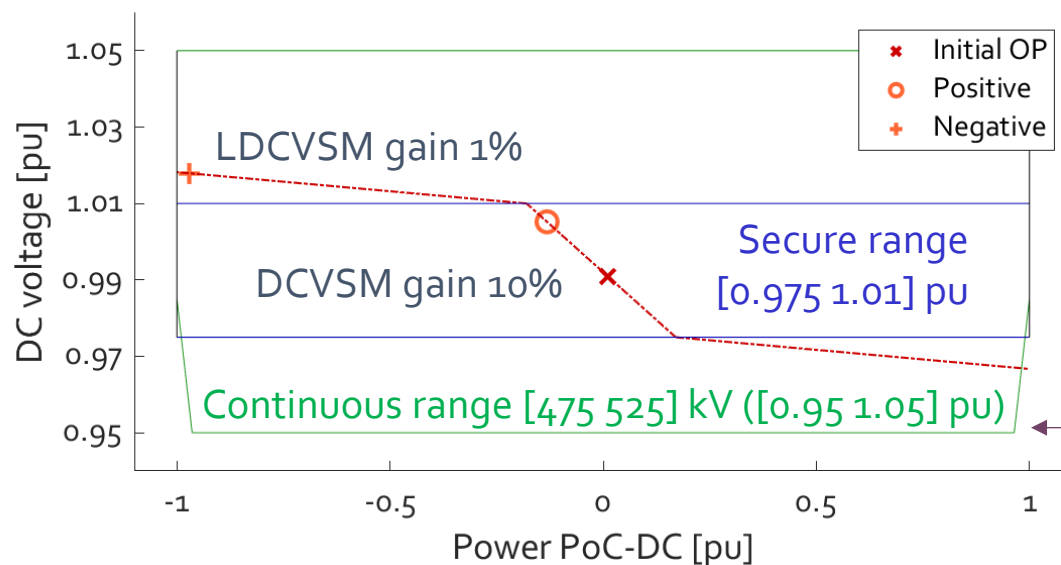
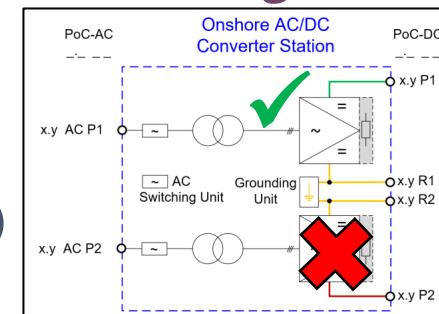
1. Define relevant scenarios, covering worst-case operating conditions
2. Compute DC voltage and power in missing nodes (through load-flow calculations)
3. Assign DC voltage control capabilities (e.g. multi-segment pole-wise droop on onshore stations)



# 1 – DC Load Flow-based design study process

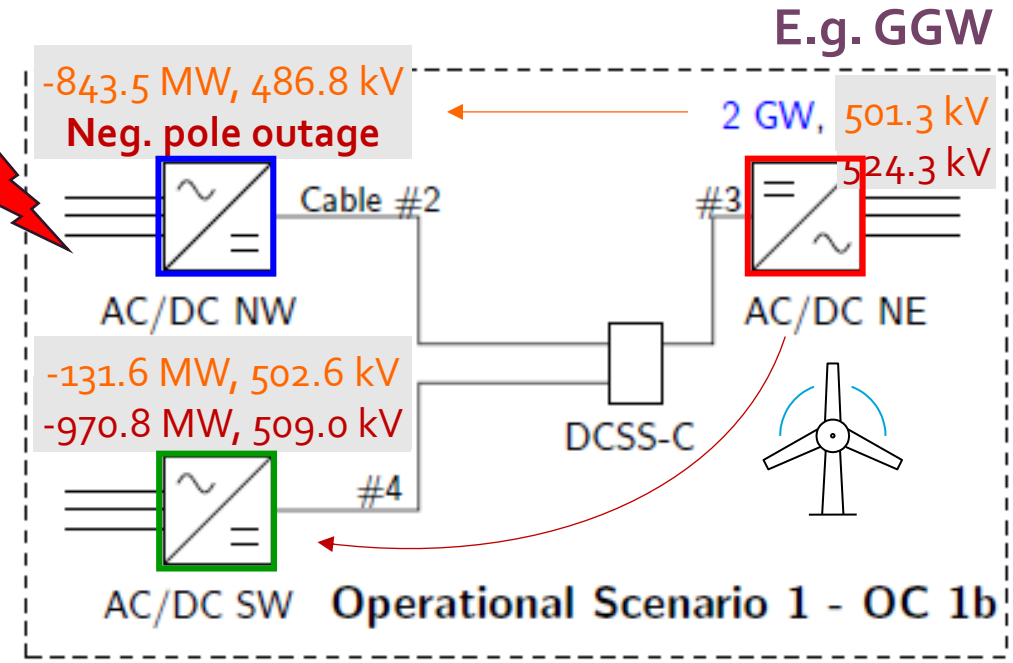
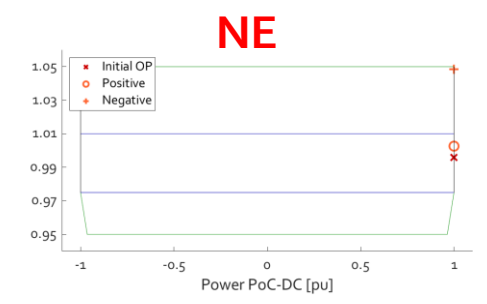
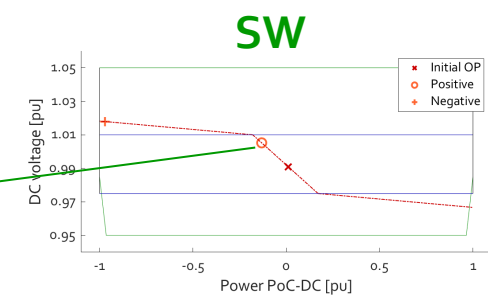
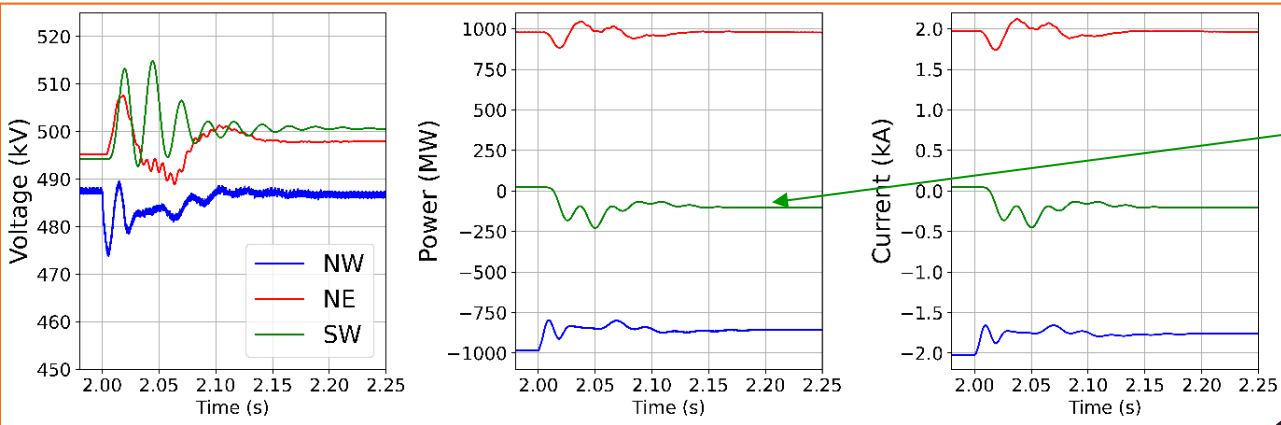
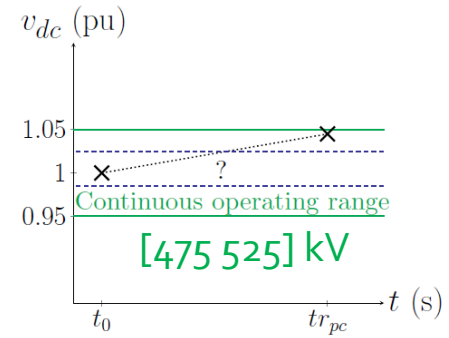
Criteria (N-1 rule): *the system must remain with the continuous range after outages*

1. Define relevant scenarios, covering worst-case operating conditions
2. Compute DC voltage and power in missing nodes (through load-flow calculations)
3. Assign DC voltage control capabilities (e.g. multi-segment pole-wise droop)
4. **Conduct contingency analysis** (propose *operational* settings: **secure range** & droop gains)



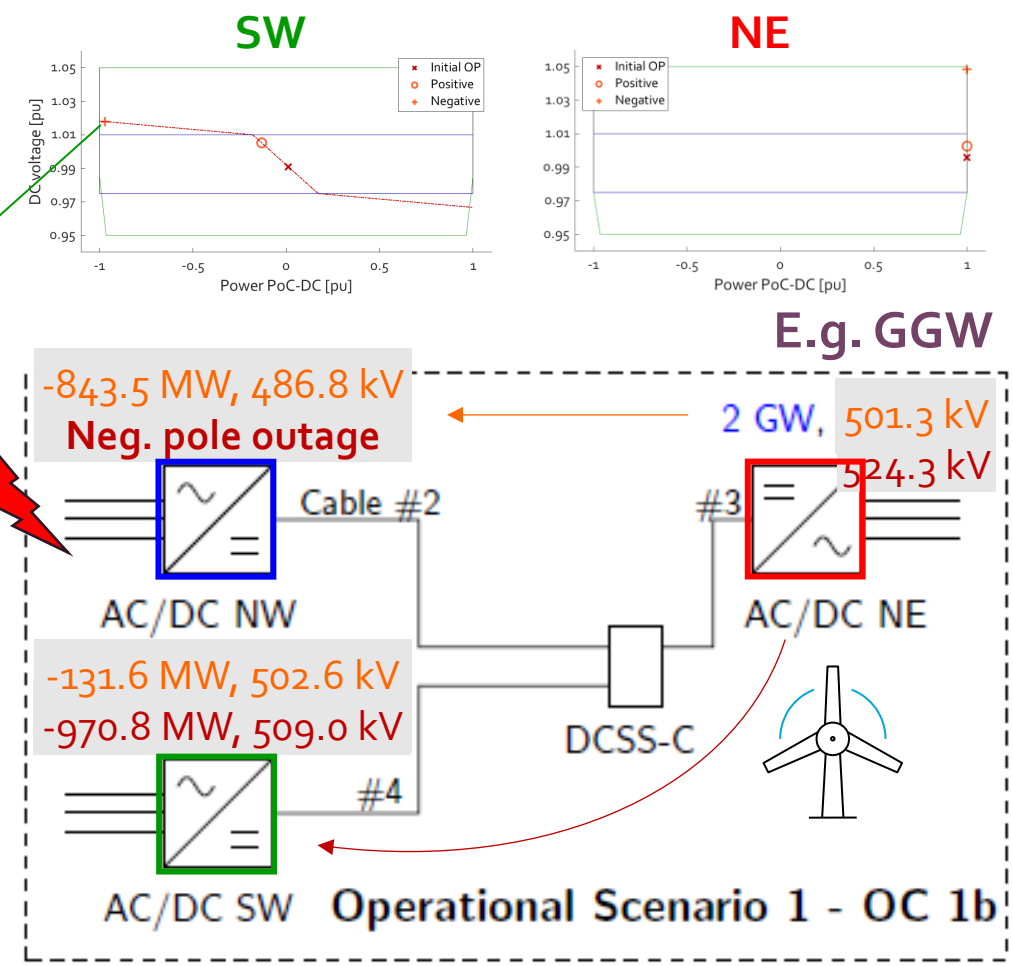
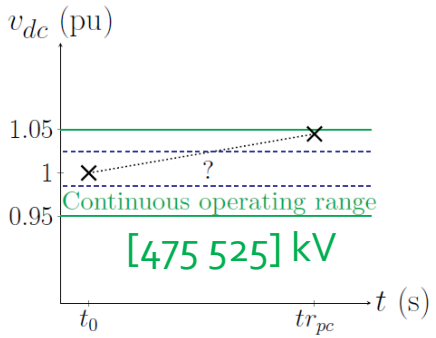
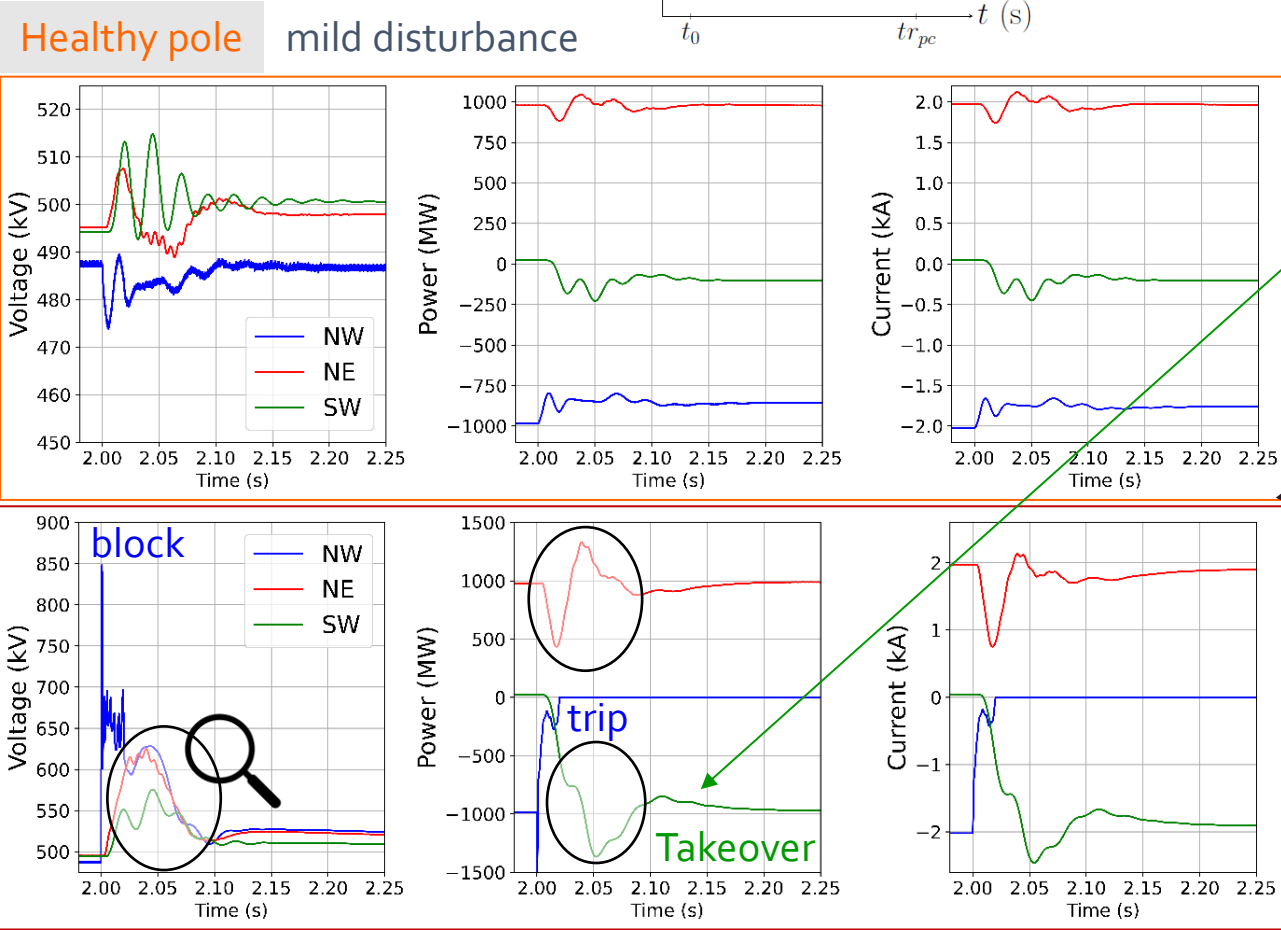
# Final states ✓ Trajectory?

Healthy pole mild disturbance



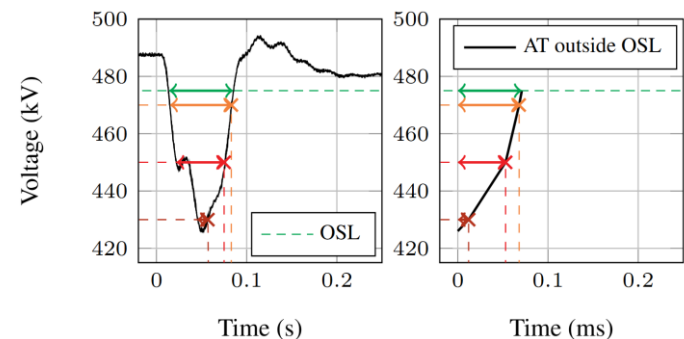
# Final states ✓ Trajectory?

# 2 – Dynamic design study! E.g., NW block & trip event

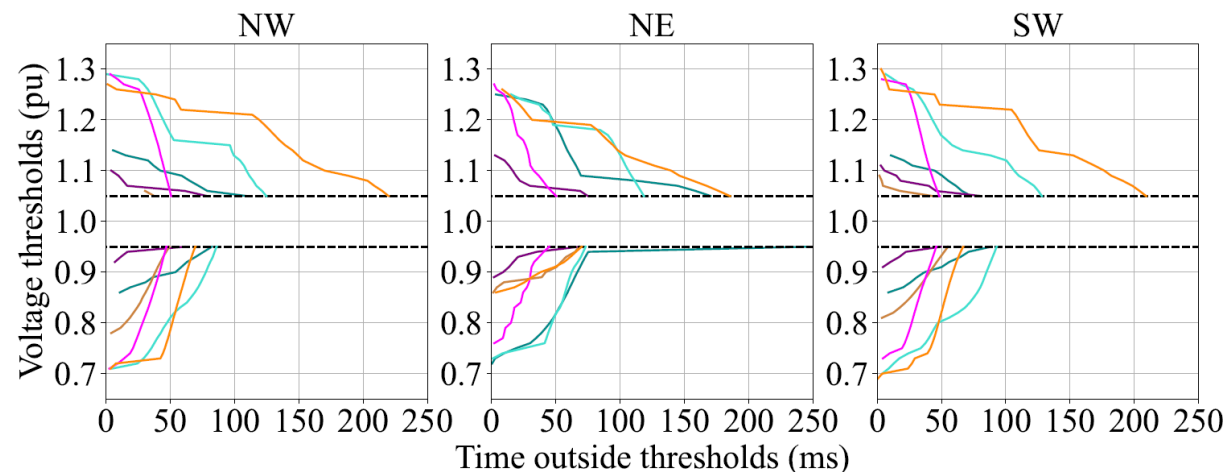


## 2 – Dynamic design study process

### Characterising stress as a function of subsystem design parameters

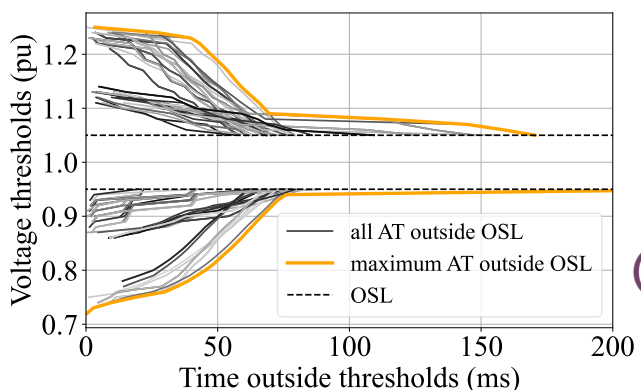


(1) Absolute Time (AT) outside OSL computed for each simulations

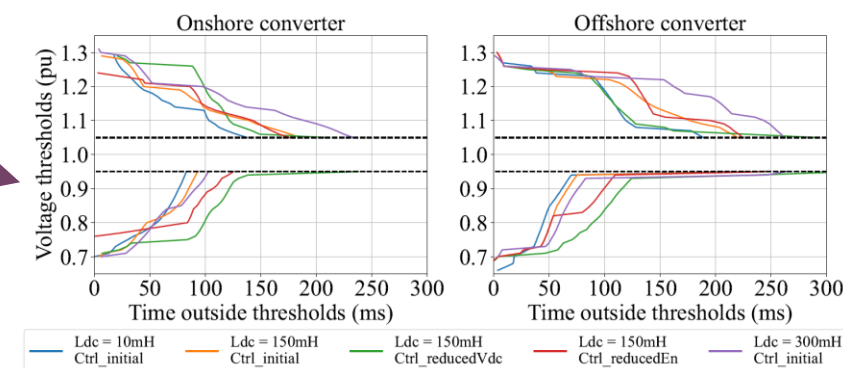


Outages & AC faults

All scenarios



(3) Envelopes are computed for each converter, event & configuration



(2) Results are aggregated, retaining the **envelope**

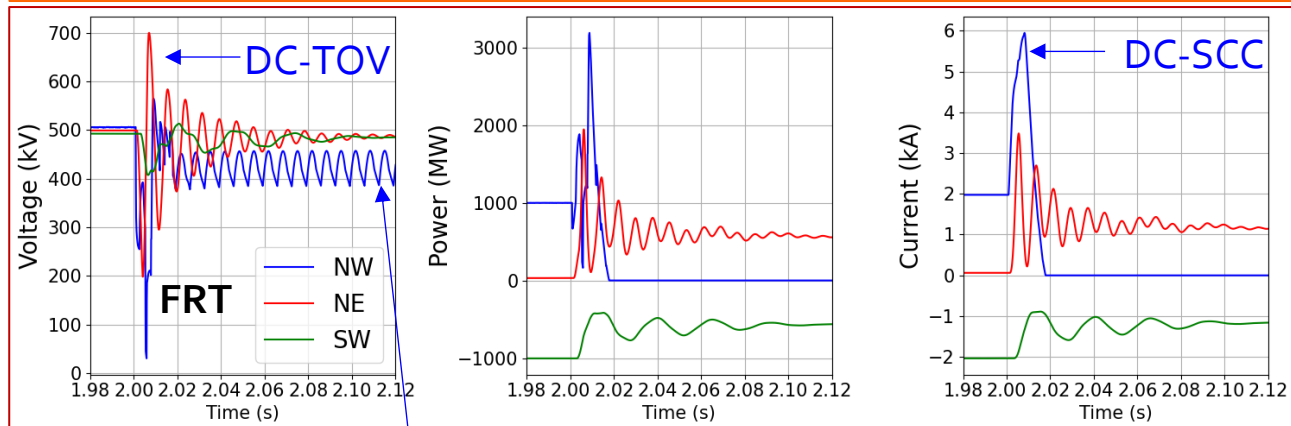
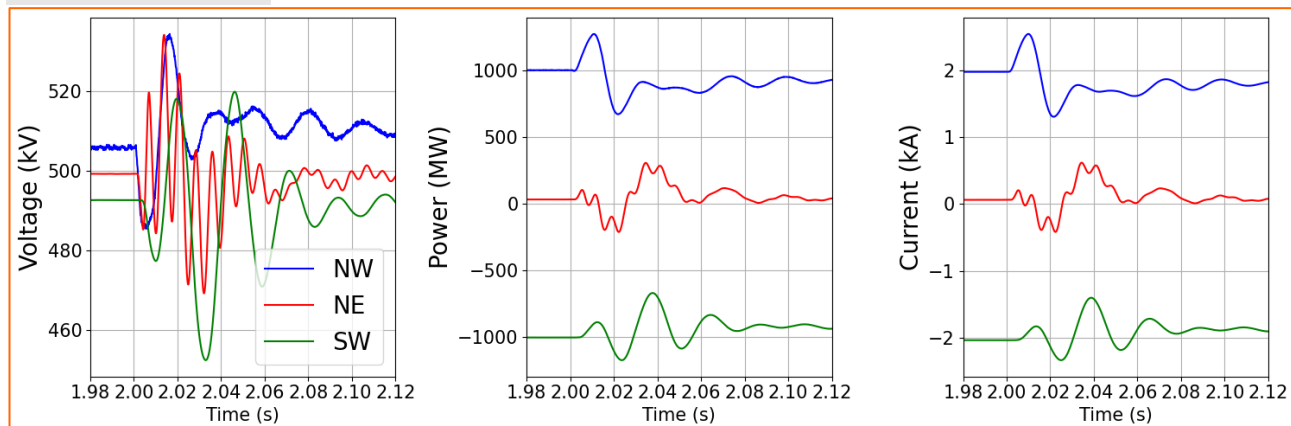
(4) Normal operation within obtained dynamic bands is specified by **station type** (onshore / offshore)



# 3 – Transient design study process: e.g. DC faults

## Compute of maximum DC short-circuit currents & overvoltages

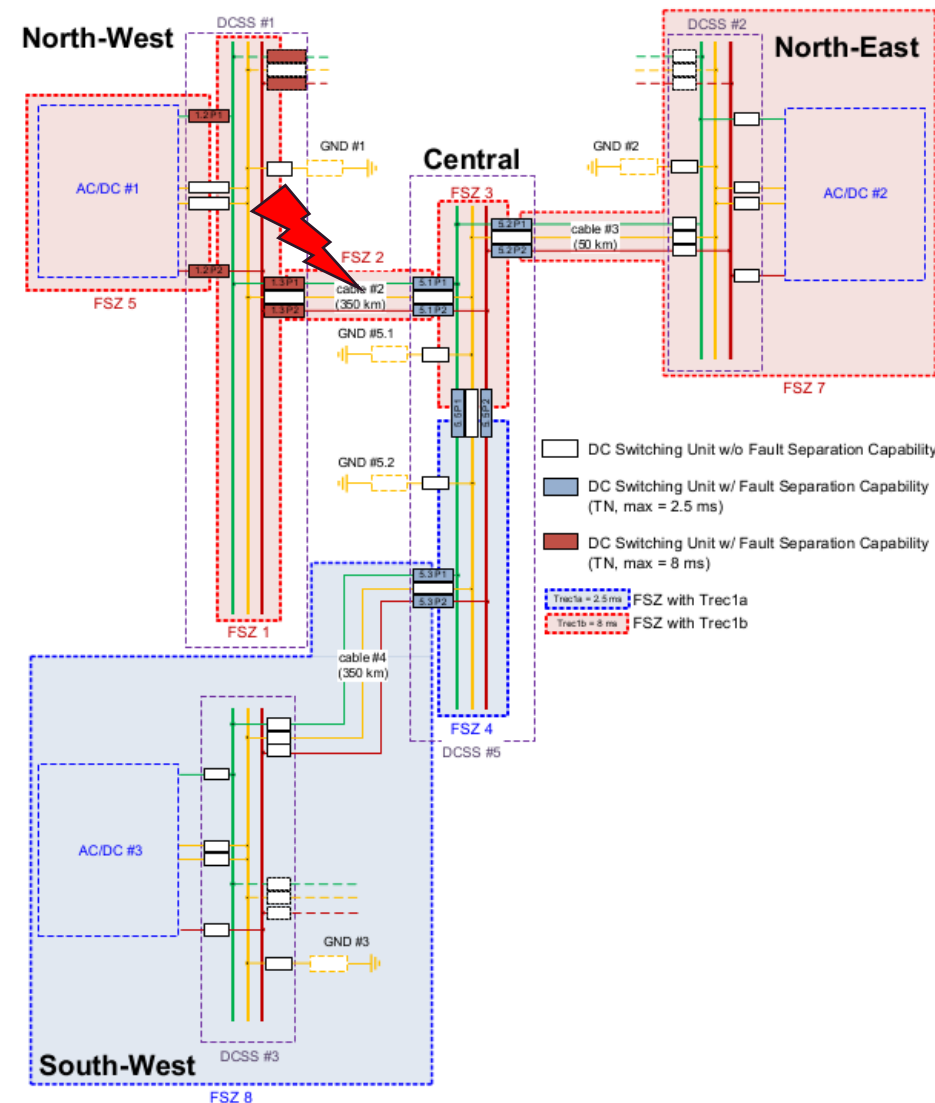
Healthy pole Limited disturbance



Affected pole

≈ few ms

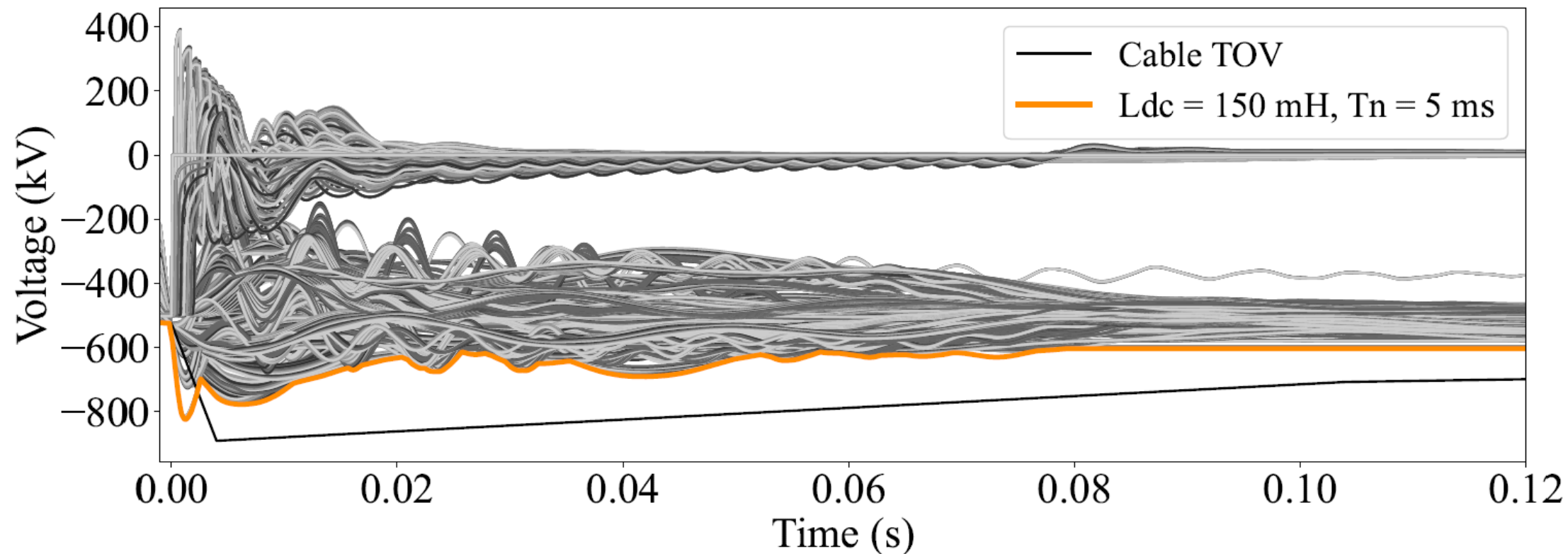
Converter (temporary) blocking





### 3 – Transient design study process: e.g. DC faults

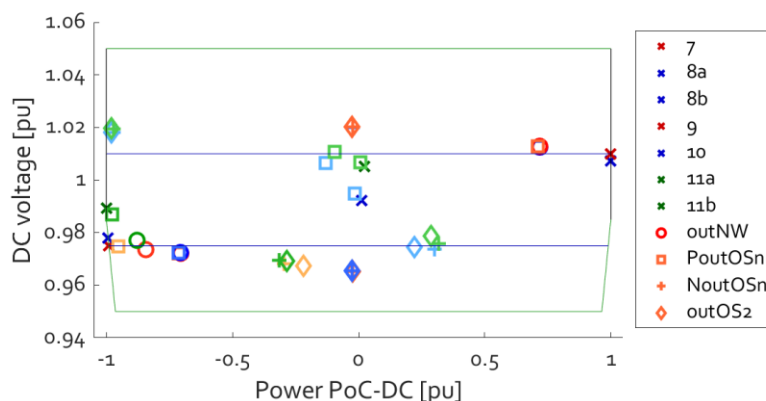
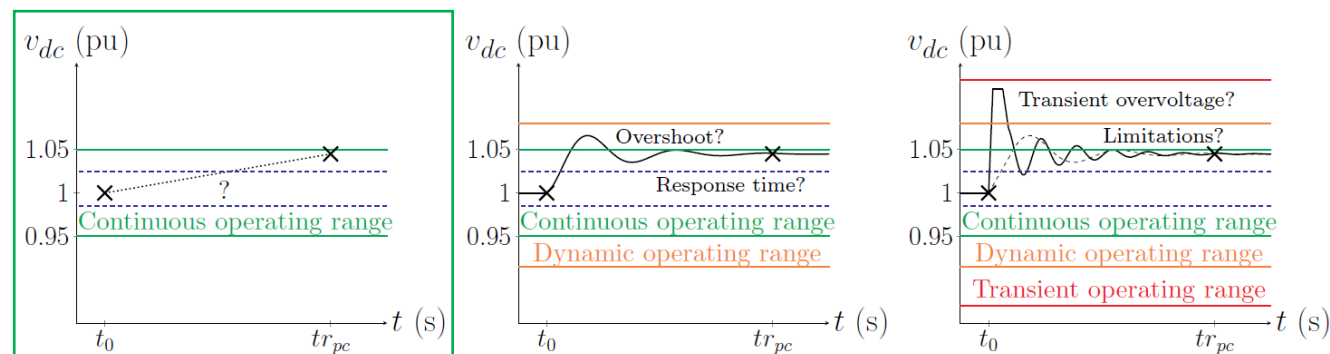
Verify compliance with the DC-TOV profile assigned to the pole cables



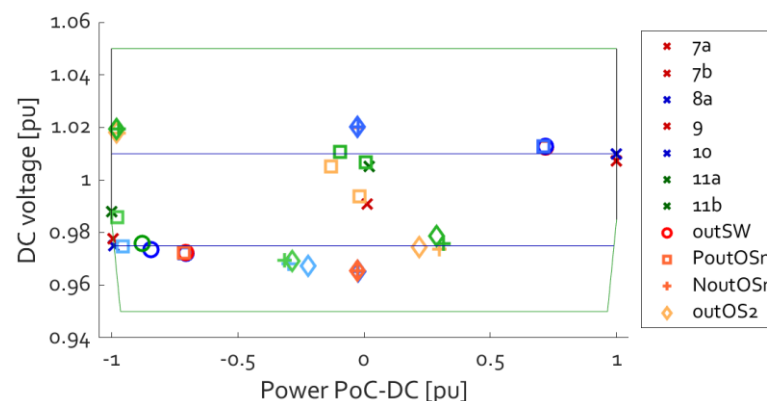
And much more...

# Takeaways

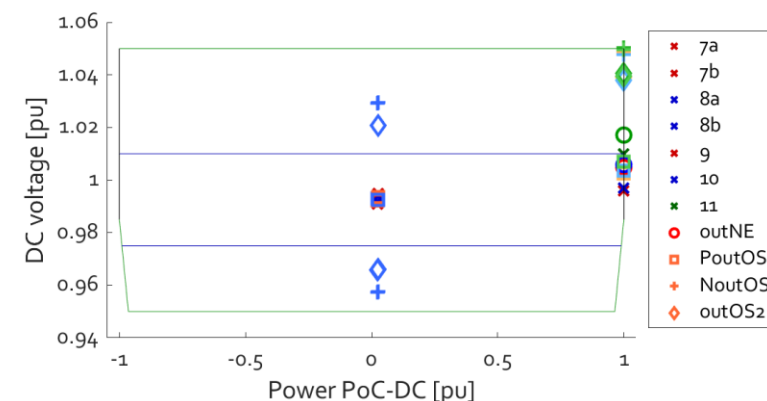
1. A general methodology for conducting HVDC grid design studies is proposed.
2. Demonstration of compatibility of **continuous operating ranges**, defined based on the ratings of currently available equipment, with the intended operational principle of the **3T InterOPERA base case** (N-1 rule).



NW (onshore)



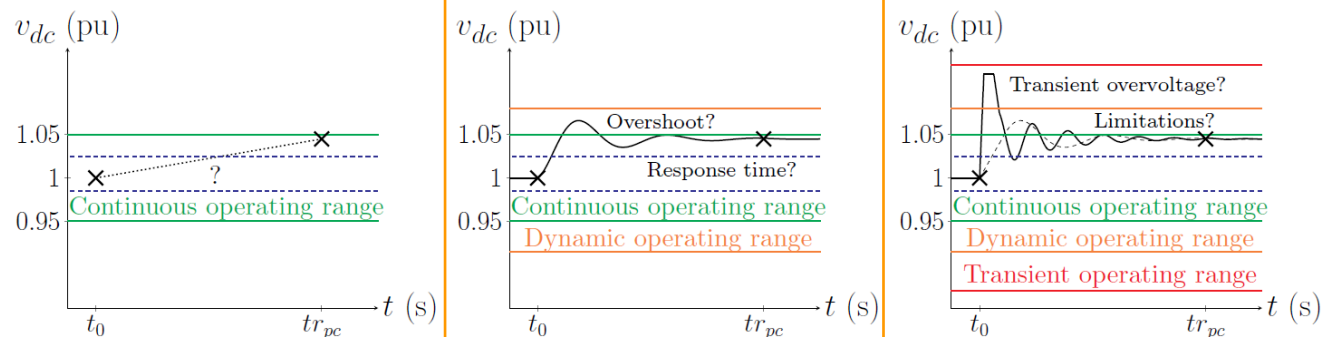
SW (onshore)



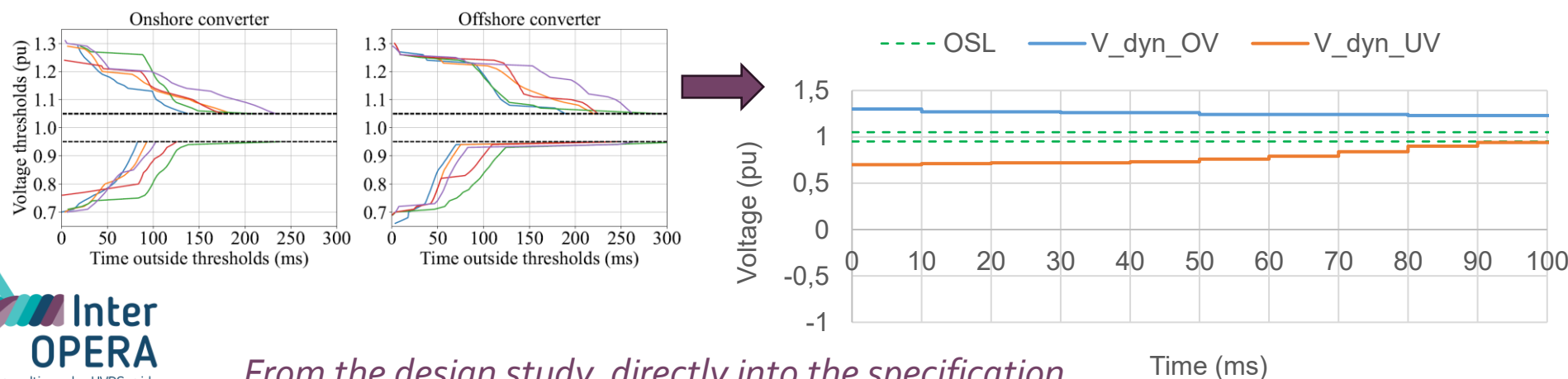
NE (offshore)

E.g. GW

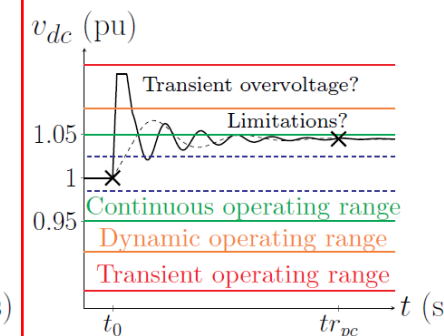
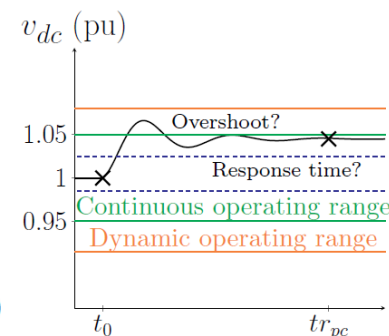
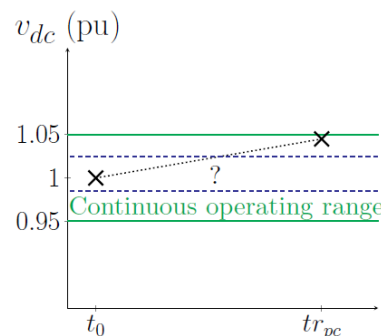
# Takeaways



1. A general methodology for conducting HVDC grid design studies is proposed.
2. Demonstration of compatibility of **continuous operating ranges**, defined based on the ratings of currently available equipment, with the intended operational principle of the **3T InterOPERA base case** (N-1 rule).
3. **Demo-specific** requirements on DC voltage **dynamic operating ranges** (no block & no trip) were defined based to the excursions observed in the design studies.



# Takeaways



1. A general methodology for conducting HVDC grid design studies is proposed.
2. Demonstration of compatibility of **continuous operating ranges**, defined based on the ratings of currently available equipment, with the intended operational principle of the **3T InterOPERA base case** (N-1 rule).
3. **Demo-specific** requirements on DC voltage **dynamic operating ranges** (no block & no trip) were defined based to the excursions observed in the design studies.
4. Validation of the proposed **withstand voltage** requirements for the InterOPERA demonstrator subsystems.

*Disclaimer: a few open questions remain...*

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24<sup>th</sup> Wind & Solar Integration Workshop | Berlin, Germany | 07-10 October 2025

## MULTI-TERMINAL MULTI VENDOR HVDC GRID DESIGN STUDIES – PART I: LOAD FLOW STUDY AND CONTINGENCY ANALYSIS

Carmen Cardozo<sup>1</sup>\*, Julien Pouget<sup>1</sup>, Hélène Clémont<sup>1</sup>, Benoît de Foucaud<sup>1</sup>, Pierre Raul<sup>1</sup>, Sébastien Dennetière<sup>1</sup>

<sup>1</sup>Electromagnetic Transients and Power Electronics, RTE, 2119 avenue Henri Schneider, 69330 Jonage, France  
\*carmen.cardozo@rte-france.com

**Keywords:** MULTI-TERMINAL HVDC, BIPOLE, DC VOLTAGE DROOP, DC LOAD FLOW

### Abstract

Multi-Terminal (MT) HVDC networks have been studied for over a decade, with recent efforts increasingly focusing on enabling multi-vendor interoperability to support a competitive and scalable deployment framework. Concurrently, protection selectivity is receiving renewed attention in the context of large-scale offshore connections based on 2 GW bipolar building blocks, where the maximum loss of infeed has become a critical planning constraint. This three-part series addresses early-stage system-level studies of MT HVDC grids using generic models, which are essential to support primary design. As part of the InterOPERA project, involving HVDC vendors traditionally responsible for DC-side design in point-to-point schemes, a methodology is proposed to instantiate project-specific technical requirements at subsystem DC point-of-connection. This first part focuses on steady-state studies to determine secure DC voltage ranges and primary control settings, ensuring N-1 compliance. For the considered three-terminal topology, different configurations of converter station connections (to onshore grids and offshore wind farms) are analysed. The case with two onshore and one offshore station exhibited the narrowest margins, prompting the definition of configuration-specific settings for the InterOPERA demonstrator. The same approach is shown to be relevant for degraded modes arising from permanent asset unavailability, with particular attention to pole-to-ground voltages under asymmetrical operation.

### 1 Introduction

Driven by the increasing scale of Offshore Wind Farms (OWFs) and the growing need for greater cross-border interconnection capacity, bipolar High Voltage Direct Current (HVDC) systems based on Modular Multilevel Converter (MMC) technology are expected to play a key role in future transmission networks. However, concerns regarding the techno-economic feasibility of relying exclusively on Point-to-Point (P2P) links have prompted the industry to address the challenges of transitioning to Multi-Terminal (MT) grids. In this context, the InterOPERA project was launched to enable future HVDC systems from different suppliers to operate together, paving the way for the actual implementation of Europe's first MT, Multi-Vendor (MV), multi-purpose HVDC projects. InterOPERA has already achieved several key milestones, including the development of common functional specifications [1] and minimum interface requirements [2]. A Real-Time (RT) demonstrator is currently being deployed to validate and refine the proposed methods and processes, ensuring their practical applicability. This work focuses on activities supporting the implementation of the RT demonstrator, particularly HVDC grid design studies using vendor-agnostic generic models, that provide input to detailed subsystem specifications.

#### 1.1 InterOPERA HVDC Grid Design Studies

The topology of the InterOPERA demonstrator, based on 2 GW bipoles, was first proposed in [3]. In parallel, general functional requirements, focusing on new DC-side capabilities to maximise interoperability by design, were jointly defined by project stakeholders [1]. Building on these inputs, detailed technical specifications for the demonstrator were developed [4], supported by dedicated system design studies that established appropriate numerical values for specific requirements. Three study packages were defined, as schematised in Fig. 1.

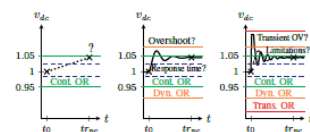


Fig. 1 Schematic representation of the scope of design studies: DC load flow and contingency analysis (left), dynamic (centre), and transient (right), with  $t_{rpc}$  the response time of the primary DC voltage control, OR Operating Range, and OV OverVoltage

1

24<sup>th</sup> Wind & Solar Integration Workshop | Berlin, Germany | 07-10 October 2025

## MULTI-TERMINAL MULTI VENDOR HVDC GRID DESIGN STUDIES - PART II: DYNAMIC STUDY

Julien Pouget<sup>1</sup>\*, Carmen Cardozo<sup>1</sup>, Pierre Raul<sup>1</sup>, Sébastien Dennetière<sup>1</sup>

<sup>1</sup>Electromagnetic Transients and Power Electronics, RTE, 2119 avenue Henri Schneider, 69330 Jonage, France  
\*julien.pouget@rte-france.com

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Multi-Terminal (MT) HVDC networks have been studied for over a decade, with recent efforts increasingly focusing on enabling multi-vendor interoperability to support a competitive and scalable deployment framework. Concurrently, protection selectivity is receiving renewed attention in the context of large-scale offshore connections based on 2 GW bipolar building blocks, where the maximum loss of infeed has become a critical planning constraint. This three-part series addresses early-stage system-level studies of MT HVDC grids using generic models, which are essential to support primary design. As part of the InterOPERA project, involving HVDC vendors traditionally responsible for DC-side design in point-to-point schemes, a methodology is proposed to refine, and eventually instantiate, project-specific technical requirements at the DC point of connection of AC/DC converters. This second part focuses on dynamic studies, quantifying maximum DC voltage excursions resulting from single and bipole outages, as well as temporary loss of power caused by converter blocking and grid-side AC faults. The variability of these excursions is examined as a function of two key design parameters: AC/DC converter reactor sizing and control settings. Time-domain simulations reveal that relatively higher stresses observed at one location are caused by large oscillations triggered by a specific blocking event. Frequency-domain assessment provides further insight into the underlying resonance phenomena.

### 1 Introduction

Driven by the increasing scale of Offshore Wind Farms (OWFs) and the growing need for greater cross-border interconnection capacity, bipolar High Voltage Direct Current (HVDC) systems based on Modular Multilevel Converter (MMC) technology are expected to play a key role in future transmission networks. However, concerns regarding the techno-economic feasibility of relying exclusively on Point-to-Point (P2P) links have prompted the industry to address the challenges of transitioning to Multi-Terminal (MT) grids. In this context, the InterOPERA project was launched to enable future HVDC systems from different suppliers to operate together, paving the way for the actual implementation of Europe's first MT, Multi-Vendor (MV), multi-purpose HVDC projects. InterOPERA has already achieved several key milestones, including the development of common functional specifications [1] and minimum interface requirements [2].

A Real-Time (RT) demonstrator is currently being deployed to validate and refine the proposed methods and processes, ensuring their practical applicability. This work focuses on activities supporting the implementation of the RT demonstrator, particularly HVDC grid design studies using vendor-agnostic generic models, that provide input to detailed subsystem specifications. Three study packages were defined, with key findings presented in this three-paper series:

- The first part establishes preliminary settings for the static characteristics of the continuous and limited DC Voltage Sensitive Modes (DCVSMs) [1], namely droop gains and boundaries for the normal (secure) operating range, derived from a DC Load Flow (LF)-based contingency analysis [3].
- This second part examines dynamic stresses at the DC Point-of-Connection (DC-POC) of various subsystems during the primary control response to selected contingencies.
- The third and final part addresses DC short-circuit currents and Temporary Overvoltage (TOV) during DC faults [4].

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#### 1.1 Background on the InterOPERA Technical Specifications

As proposed in [5], the InterOPERA demonstrator adopts a bipolar configuration rated at 2 GW per converter station (1 GW per pole). The detailed technical specifications [6], developed jointly by project stakeholders, introduce new DC-side requirements, most notably DC voltage operating ranges and primary DC voltage control specifications in line with [1]. Additionally, dedicated system design studies were conducted to establish appropriate numerical values for these requirements as applied to the InterOPERA demonstrator.

Specifically, dynamic performance requirements for the primary DC voltage control are expressed in terms of characteristic indicators such as rise time, settling time, response time, and overshoot. These apply to individual subsystems, namely AC/DC converter stations, with compliance verified through standalone tests using well-crafted grid equivalents [1]. When considering grid-connected investigations, three types of studies must be distinguished:

- HVDC grid design studies with generic models; the focus of this work;
- Control development within detailed subsystem design and the Original Equipment Manufacturer (OEM) scope; and
- Interaction studies conducted at the integration stage using vendor models [7].

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## MULTI-TERMINAL MULTI VENDOR HVDC GRID DESIGN STUDIES – PART III: TRANSIENT STUDY

Benoît de Foucaud<sup>1</sup>\*, Julien Pouget<sup>1</sup>, Carmen Cardozo<sup>1</sup>, Pierre Raul<sup>1</sup>, Ambroise Petit<sup>1</sup>, Sébastien Dennetière<sup>1</sup>

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**Keywords:** MULTI-TERMINAL HVDC, BIPOLE, DCCBs, DC TOV, DC SHORT-CIRCUIT CURRENT

### Abstract

Multi-Terminal (MT) HVDC networks have been studied for over a decade, with recent efforts increasingly focusing on enabling multi-vendor interoperability to support a competitive and scalable deployment framework. Concurrently, protection selectivity is receiving renewed attention in the context of large-scale offshore connections based on 2 GW bipolar building blocks, where the maximum loss of infeed has become a critical planning constraint. This three-part series addresses early-stage system-level studies of MT HVDC grids using generic models, which are essential to support primary design. As part of the InterOPERA project, involving HVDC vendors traditionally responsible for DC-side design in point-to-point schemes, a methodology is proposed to refine, and eventually instantiate, project-specific technical requirements at subsystem DC point-of-connection. This third part focuses on transient studies, quantifying maximum DC short-circuit currents and overvoltages induced by pole-to-ground faults throughout the fault separation process. The variability of system-level electrical stress is assessed as a function of two key design parameters: AC/DC converter reactor sizes and DC circuit breaker's maximum fault neutralisation times. Broader discussions on insulation coordination considerations and DC fault ride-through requirements are also provided.

### 1 Introduction

Driven by the increasing scale of Offshore Wind Farms (OWFs) and the growing need for greater cross-border interconnection capacity, bipolar High Voltage Direct Current (HVDC) systems based on Modular Multilevel Converter (MMC) technology are expected to play a key role in future transmission networks. However, concerns regarding the techno-economic feasibility of relying exclusively on Point-to-Point (P2P) links have prompted the industry to address the challenges of transitioning to Multi-Terminal (MT) grids. In this context, the InterOPERA project was launched to enable future HVDC systems from different suppliers to operate together, paving the way for the actual implementation of Europe's first MT, Multi-Vendor (MV), multi-purpose HVDC projects. InterOPERA has already achieved several key milestones, including the development of common functional specifications [1] and minimum interface requirements [2].

A Real-Time (RT) demonstrator is currently being deployed to validate and refine the proposed methods and processes, ensuring their practical applicability. This work focuses on activities supporting the implementation of the RT demonstrator, particularly HVDC grid design studies using vendor-agnostic generic models, that provide input to detailed subsystem specifications. Three study packages were defined, with key findings presented in this three-paper series: Part I introduces a DC Load Flow (LF)-based contingency analysis [3], while Part II examines the system dynamic response following unit outages [4]. This third part addresses transient electrical stresses at the DC Point-of-Connection (DC-POC) of various subsystems during

and following DC faults. As introduced in the companion papers [3, 4], InterOPERA adopts a bipolar configuration rated at 2 GW per converter station with DC fault-handling capabilities [5]. DC Switching Units (DCSUs) equipped with DC Circuit Breakers (DCCBs) are implemented in selected DC Switching Stations (DCSSs), incorporating reactors to limit the fault current rise rate and enable fault separation. As illustrated in Fig. 1, the inclusion of DCCBs introduces the concept of Fault Separation Zones (FSZs), requiring parts of the system to withstand and recover from external DC faults; a structural assumption that significantly influences the results presented in this work. This notably implies that AC/DC converters must comply with DC-Fault Ride-Through (DC-FRT) requirements, which may necessitate revisiting their design. Although two topologies are considered in the project: a Three-Terminal (3T) and a Five-Terminal (5T) DC grid, both including a central DCSS, this paper series focuses on the 3T base case.

#### 1.1 Background on Transient DC-side Requirements

In practice, the solutions delivered by vendors are developed to comply with contractually binding technical specifications. Transient DC interface requirements, typically expressed in terms of Short-Circuit Current (SCC) and DC-Temporary Overvoltage (TOV), have been incorporated into the specifications of P2P HVDC projects due to the separation of converter station and cable procurement processes. These requirements are generally derived from pre-design studies supported by Electromagnetic Transient (EMT) simulations, using generic models tailored with project-specific assumptions.

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# THANK YOU

# Closing remarks:

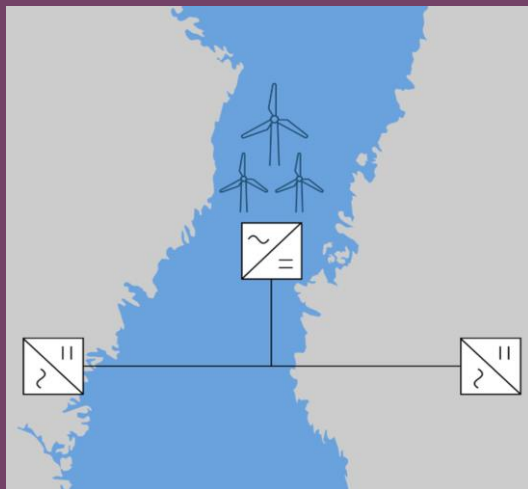
## How InterOPERA is contributing to the EU's energy goals

Supporting frameworks for a more integrated European energy market



# Context & what InterOPERA Delivers for Europe

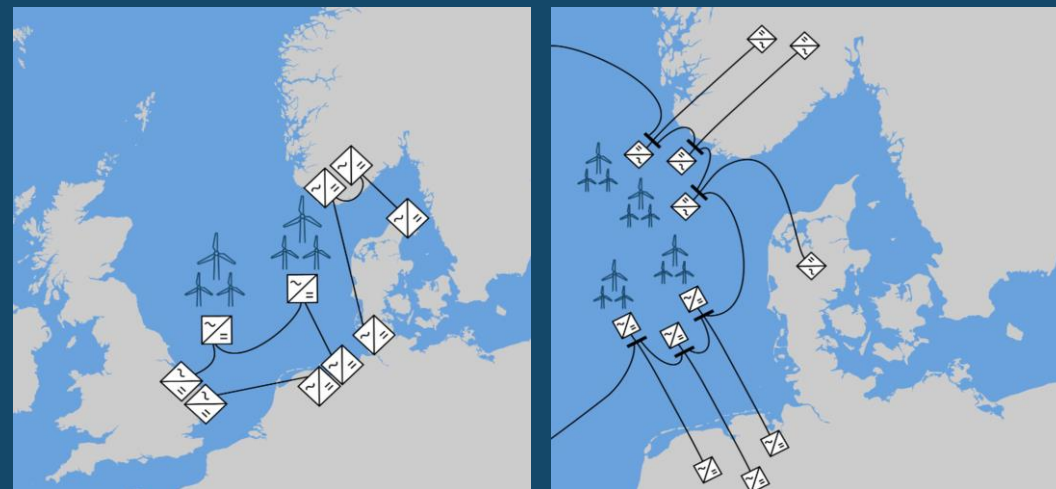
Today



**HVDC projects bespoke and fragmented**  
**Risk in developing multi-vendor systems**  
**Need for Interoperable HVDC Grids**



Tomorrow



**Common functional requirements and standards**  
**Multi-vendor & multi-terminal Interoperability**  
**Delivers frameworks for procurement, IP, fair competition**



# Impact on Policy and Market Readiness

## Standardization and Harmonization

Contributes to harmonizing connection codes and procurement practices across European and international standards bodies.

## Market Readiness and Competition

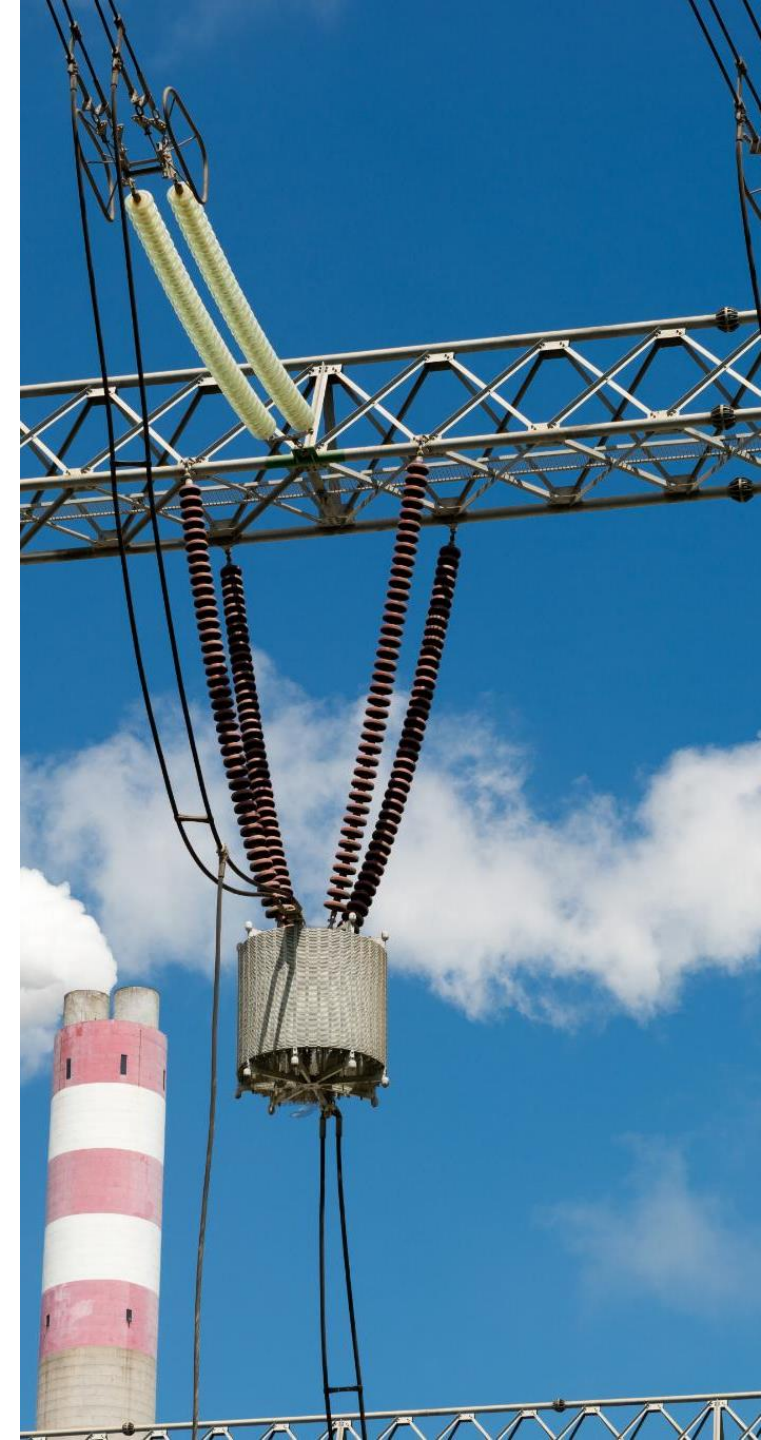
Harmonized standards enable a competitive multi-vendor market, reducing project risks and accelerating deployment.

## Regulatory Support and Policy Integration

Provides validated methodologies that support regulatory uptake and integration into EU and national frameworks.

## Facilitating HVDC Tenders

Common standards and procurement frameworks enable the launch of HVDC multi-terminal system tenders.



# The Exploitation Plan Heritage of InterOPERA

## Ensuring Continuity and Adoption

The plan guarantees continuity through adoption of standards, procurement processes, and regulatory frameworks.

## Integration into Commercial and Policy Sectors

Strategies focus on embedding InterOPERA's outputs into future commercial projects and policy instruments.

## Intellectual Property Protection and Fair Competition

Promoting multi-party cooperation while protecting intellectual property.

## Supporting Sustainability and Scalability

Transforms project innovations into deployable solutions for a sustainable and scalable HVDC infrastructure across Europe.





# A Lasting Legacy for Europe's Offshore Grid

## **Legacy of Collaboration**

InterOPERA promotes shared standards and open collaboration to support Europe's energy transition.

## **Interoperability and Infrastructure**

Enabling interoperability across HVDC systems creates scalable and efficient offshore grid infrastructure.

## **Policy and Market Readiness**

Contributions to policy and market readiness ensure Europe meets climate goals while securing energy resilience.

## **Driving Systemic Change**

Collaborative innovation drives systemic change, positioning InterOPERA as a cornerstone of future energy.

# THANK YOU

# InterOPERA Phase II

## What's coming next

Launching real-world testing with a physical demonstrator to prove system interoperability

Supporting future commercial deployment of multi-vendor offshore energy systems in Europe

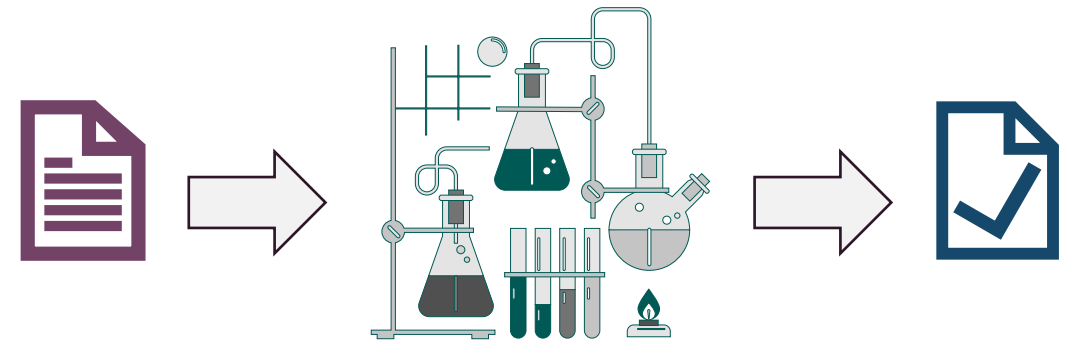
# 1

Launching real-world testing  
with a physical demonstrator to  
prove system interoperability

# Why Use a Demonstrator?

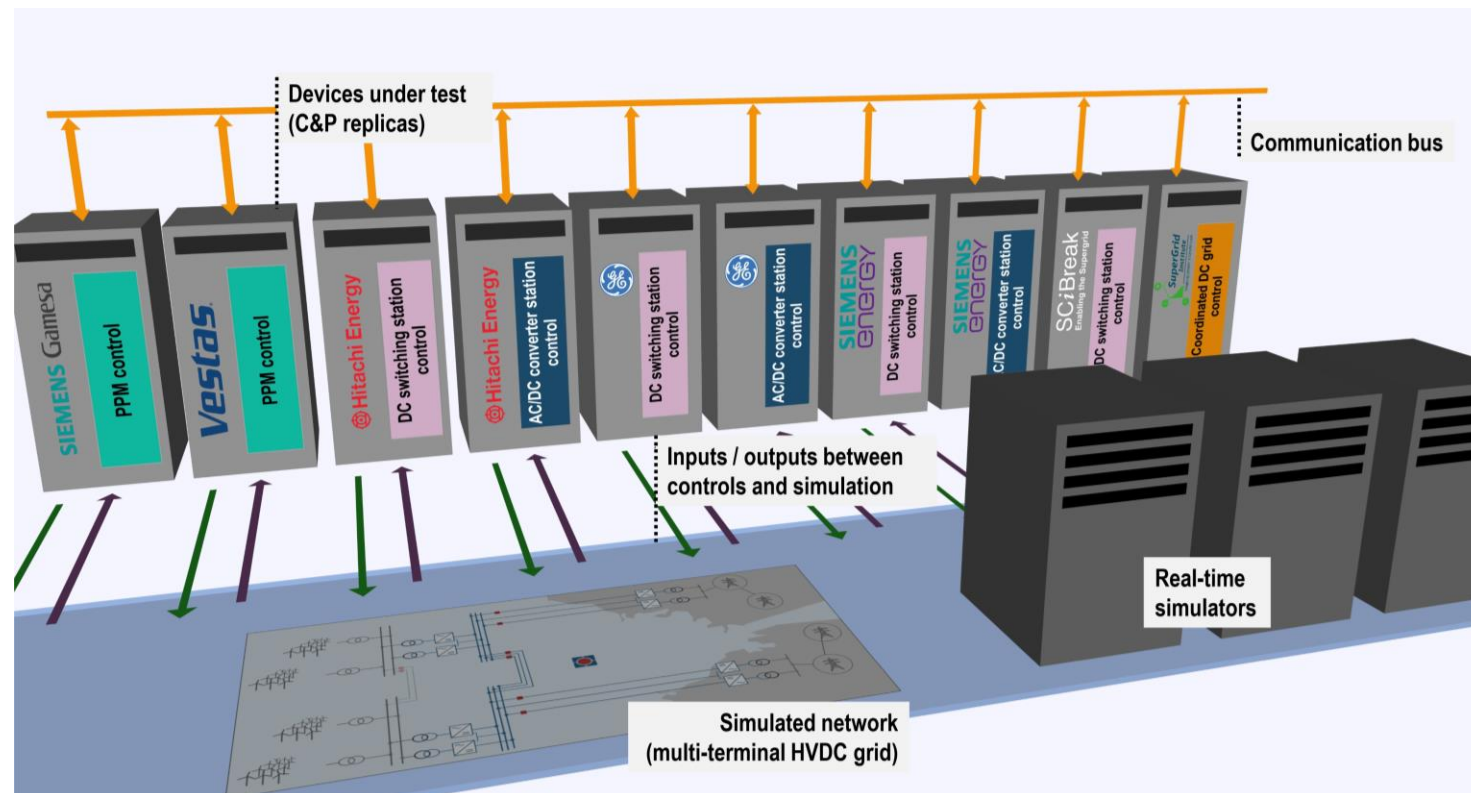
- Phase I:
  - **Defined functional requirements** for multi-vendor interoperability
- Phase II:
  - Can **real vendor hardware** meet those requirements under **realistic conditions**?
  - Put **verifiable requirements** into **template specification** to be used in future tenders

➤ De-risk future multi-vendor projects



# Multi-Terminal Multi-Vendor HVDC Real-Time Demonstrator (Overview)

- Validation for Control & Protection System Interoperability
  - Laboratories:
    - RTE (FR)
    - TU Delft (NL)
  - Goal: One coherent DC grid controlled by independent vendors' equipment
- What will we test with it?

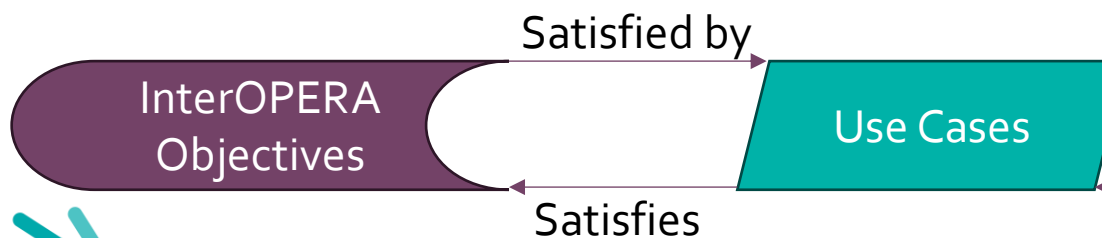


\*Mitsubishi to provide DC protection for the DCCB



# Demonstrator Use Cases

- Use Case definition template
  - Category & priority rating
  - Preliminary or final specs (D3.3)
  - Description
  - Min. required grid topology, config or equipment
  - Minimum D3.1 subset
  - Simulation environment (testing method)
  - Pre-Condition → Trigger → Post-Condition
  - Primary / Alternative / Failure flow
  - Actors / involved subsystems



Grid Operation and Reconfiguration
Start-up from 1 onshore station and shut-down
Transition from one power flow schedule to another (only set points)
Transition to new control modes and control parameters
Basic switching operations and grid reconfiguration sequences
Secondary control - automatic transition to a new power flow schedule after a severe contingency
Planned subgrids merge - on load switching
Planned grid split - on load switching
Continuous Controls
Power disturbance with 1 converter station in Vdc control mode, the others in power control mode
Power disturbance with converter stations in Vdc-droop control modes
Asymmetrical pole operation due to one transmission pole outage
Asymmetrical pole operation due to difference in power injection in positive and negative poles
Vdc-droop converters connected to the same DC-bus, to the same DC switching station
DC Protection
DC fault within all selective fault separation zones
DC fault within the fault separation zone including non-selective zones
Offshore AC Performance
Offshore grid energization from 1 offshore HVDC station ("soft start")
PPMs from two different vendors connected to the same busbar (steady-state small-signal operation validation)
Reconfiguration of the offshore AC network, energizing one part from the other by closing a switch ("hard start")
Ride through offshore HVDC converter temporary blocking with WTGs in GFL control mode
HVDC converter permanent blocking with WTGs in GFL control mode
DC-side contingency leading, after energy absorber activation, to a coordinated emergency offshore wind ramp-down or curtailment
Offshore AC fault ride through capability with GFL WTGs - Post fault active power recovery
Onshore AC Performance
Onshore AC fault ride through capability - Post fault active power recovery
Reactive power control, including priority management with active power control
Inertia support (GFM control scheme with inertia support from one asynchronous area to another)
Exploration of HVDC system stability and interoperability with interconnected AC areas (no design requirements)

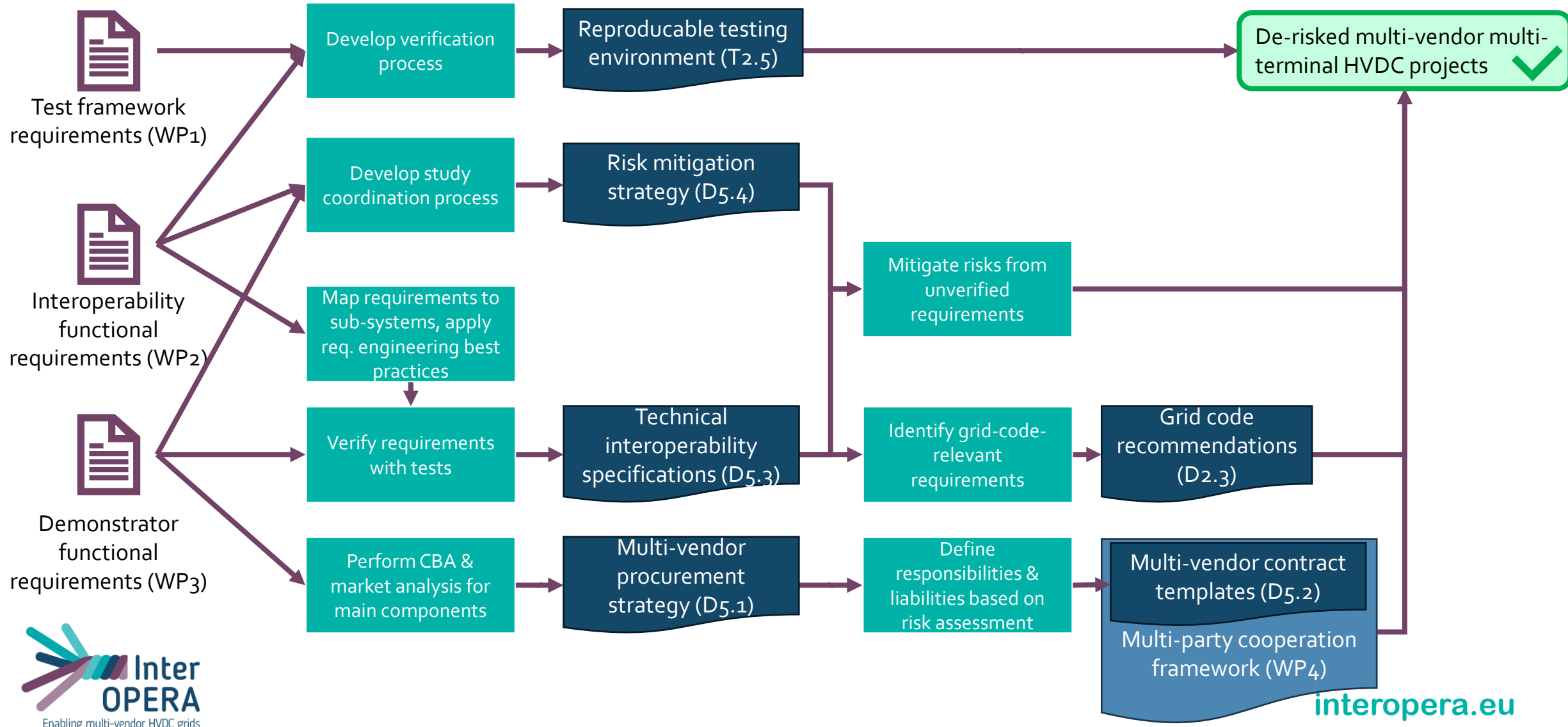
# How To Test Interoperability

- “Dry-run” tests
  - Check vendor **models’ consistency** with defined requirements
  - Describe **how to provide** models & replicas (IEEE/Cigré DLL)
  - **No** focus on dynamic behaviour
  - Expected to finish by end of 2025
- Interaction tests
  - **Define tests** covering the use cases
  - **Test requirements** developed in the project
  - Assess if requirements (and corresponding standalone tests) are sufficient for guaranteeing **interoperability by design**
  - **Offline EMT** models validate steady-state & fault calculations
  - **Hardware-in-the-Loop** runs the actual control cubicles in real-time for key scenarios

# 2

Supporting future commercial  
deployment of multi-vendor  
offshore energy systems in  
Europe

# Developing a multi-vendor tender template



# Multi-Party Cooperation Framework

## The road to successful MTMV HVDC projects

The aim of the Multi Party Cooperation Framework is to facilitate the cooperation with regards to;

*the development and operation of multi-vendor, multi-terminal high-voltage direct-current grids (MVMTHVDC grids).*

- Ensure the first MTMV HVDC project has the right setup for multi party collaboration
- Ensure that the Multi Party Cooperation Framework can support the chosen tender process.
- Enable pre-tender and post contract award collaboration through the multi-party collaboration framework
- Allow for collaboration on a detailed engineering level to de-risk the project from conception phase onwards
- Confidentiality provisions are taken into account
- Ensure European competition law is adhered to
- Protect Intellectual Property of vendors adequately

# Multi-Party Cooperation Framework

The current aim, as formulated in the draft MPCF is to facilitate the cooperation of the Parties and other stakeholders in connection with the development and/or operation of multi-vendor, multi-terminal high-voltage direct-current grids (MVMT HVDC grids).

## Within InterOpera



## Post InterOpera



Phases	Lead	Competitive dialogue	Restricted procedure
Concept design	TSO		Required
<b>Pre-qualification – definition of pre-qualification requirements – MPCF as a requirement to pre-qualify?</b>			
Pre-FEED/Feasibility study (applicable in restricted procedure)	TSO		Required with input from pre-qualified parties
Basis for design, lot allocation, functional requirements	TSO		Required with input from pre-FEED basis
Competitive dialogue – coordination studies	TSO + Bidders	Required	Not Applicable
<b>Publication of contract notice / ITT</b>			
Tender	Bidders		Required
<b>Contract Award (conditional to investment decision after FEED)</b>			
FEED study	TSO + contractors		
<b>Financial Investment Decision (which is linked to OFW tender)</b>			
Detailed Engineering	Contractors		
Procurement	Contractors		
Construction	Contractors		
Installation	Contractors		
Commissioning	Contractors + TSO		
<b>Take-over</b>			
Operation and maintenance	TSO		
Infrastructure extension/lifetime ext./decommissioning			

# InterOpera demonstrator

## Accelerated learning, unlocking the essential collaborative setup

- First draft of the Multi Party Cooperation Framework was published end '24.
- Maximize learning from implementation of the demonstrator
- Continuous learning to improve the collaboration framework and taking these learnings into new versions of the MPCF
- Ensuring that the MPCF will support future MTMV HVDC projects in the best possible way
- Coupling the framework to the lifecycle of an MTMV HVDC project

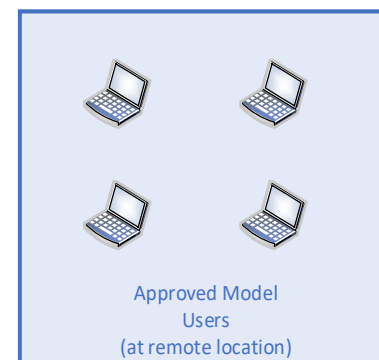
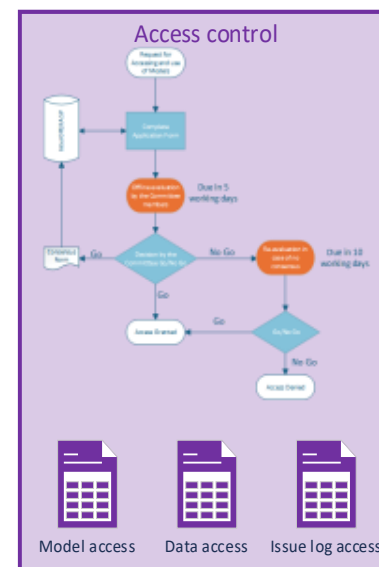
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Installation	Contractors		
Commissioning	Contractors + TSO		
Take-over			
Operation and maintenance	TSO		
Infrastructure extension/lifetime ext./decommissioning			

# Post InterOpera outlook

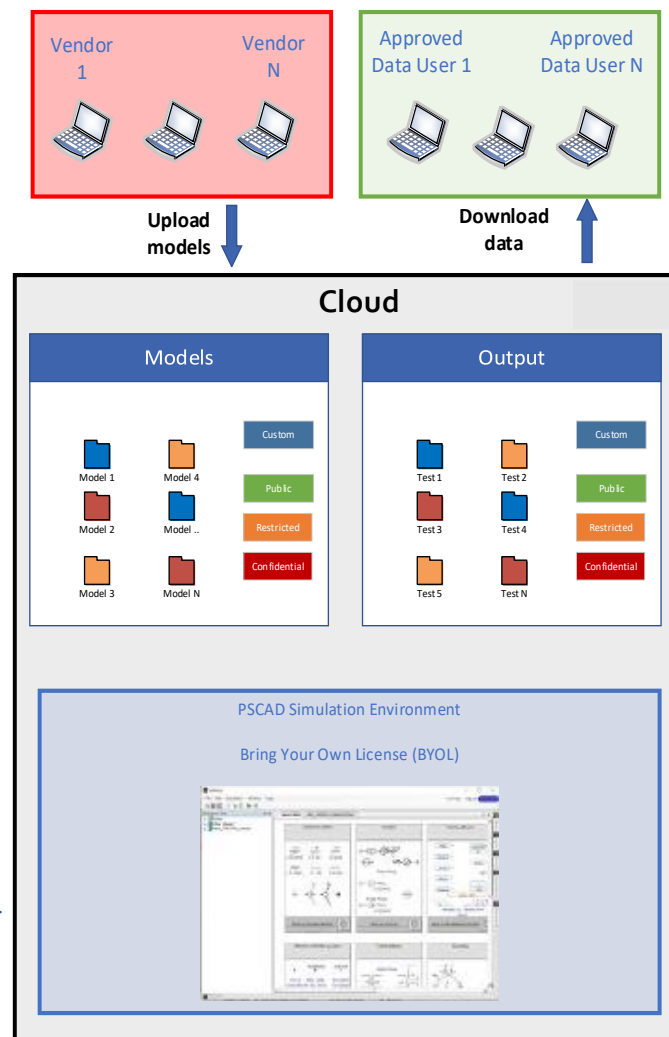
## A hosted collaboration platform for pre-tender coordination studies

Target is to develop a system where MTMV coordination studies can be executed optimally whilst ensuring confidentiality, without the need for elaborate bi-lateral legal provisions

- Storage of models, data and other information will be in the cloud
- Decentralised access control, ensuring all parties are in control of access to their own models and data
- TSOs, vendors and other approved users can log in to a dedicated cloud computer to jointly perform simulations which would not require any download of models or sensitive information.
- Limiting legal agreements to be in place with governance ideally treated within agreed MPCF.
- General development and maintenance cost of such a collaboration platform is cost heavy and requires dedicated governance and secure hosting.



Remote  
desktop/  
VPN access





# Concluding remarks

- Learnings on the demonstrator are beyond the technical understanding of the system alone.
- Learnings from the demonstrator on the collaboration will be key to successful implementation of a collaboration framework for the first MTMV HVDC project.
- A combination of legal and practical implementations will enable successful MTMV HVDC collaboration
- With InterOpera we are on a steep learning curve, where phase 2 of the project will bring essential experience for the realisation of the first MTMV HVDC project.

# Timeline & Next Milestones

